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Dominion Resources Services, Inc. 5000 Dominion Boulevard, Glen Allen, VA 23060 Web Address: www.dom.com

December 29, 2014

## BY: U.S. CERTIFIED MAIL, RETURN RECEIPT REQUESTED

7012 3460 0003 4189 7904

William F. Durham Director, Division of Air Quality WVDEP 601 57<sup>th</sup> Street Charleston, WV 25304

#### RE: <u>Dominion Transmission, Inc. – General Permit (G35-A) Application</u> <u>Big Isaac Compressor Station</u>

Dear Mr. Durham:

Enclosed are one complete original and two (2) copies of a G35-A General Permit application for the proposed replacement of the existing flare at Dominion Transmission, Inc.'s Big Isaac Compressor Station in Doddridge County, West Virginia.

The public notice affidavit will be submitted to WVDEP once it is received from the newspaper.

If you require any additional information, please contact Rebekah Remick at (804) 273-3536 or via email at Rebekah.J.Remick@dom.com.

Sincerely,

Amanda B. Tornabene Director, Gas Environmental Services





## APPLICATION FOR CLASS II G35-A GENERAL PERMIT

DOMINION TRANSMISSION, INC. BIG ISAAC STATION FACILITY ID NO. 017-00029

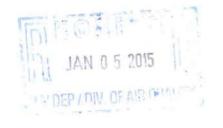
Submitted By:



**DOMINION TRANSMISSION, INC.** 445 West Main Street Clarksburg, WV 26301

Prepared By:





Submitted To:



WEST VIRGINIA DEPARTMENT OF ENVIRONMENTAL PROTECTION Division of Air Quality 601 57<sup>th</sup> Street, SE Charleston, WV 25304

Submitted: December 2014

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#### 1. INTRODUCTION

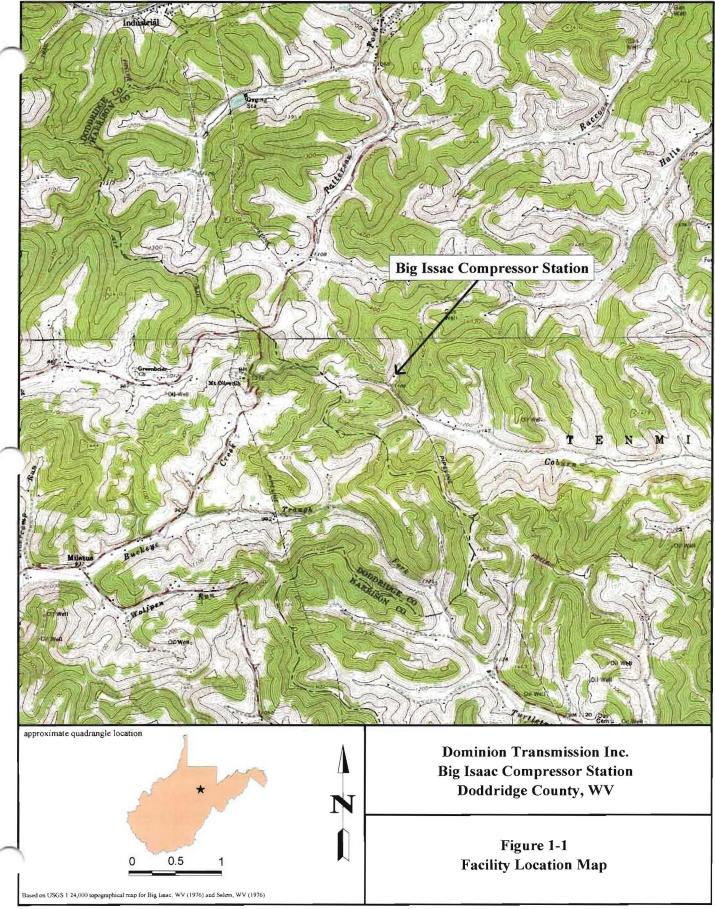
Dominion Transmission, Inc. (Dominion) specializes in gas transmission and storage services. The Big Isaac Compressor Station (Station) is an existing natural gas compressor station that pumps natural gas from production and gathering lines to a Dominion pipeline. The Station uses one (1) glycol dehydration unit to remove water from wet natural gas and transports the natural gas to a natural gas processing plant. Dominion is proposing to replace the existing flare at the Station. The flare serves as an air pollution control device for the glycol dehydration unit.

#### 1.1 EXISTING BIG ISAAC COMPRESSOR STATION

The Station is located in Doddridge County, West Virginia. Figure 1-1 shows the general location of the Station on sections of the Big Isaac and Salem, West Virginia, United States Geological Survey (USGS) quadrangles. The major source thresholds for the West Virginia Title V operating permit program regulations are 10 tons per year (tpy) of a single hazardous air pollutant (HAP), 25 tpy of any combination of HAP, or 100 tpy of all other regulated pollutants. The Station does not have the potential to emit over 100 tpy of any pollutant, nor does the Station emit any individual HAP or any combination of HAPs above the 10 tpy and 25 tpy thresholds respectively. Therefore, the Station is classified as a nonmajor source for Title V purposes and is classified as an area source of HAPs. Because the Station is not a major source, it is not required to have an operating permit pursuant to Title V of the Federal Clean Air Act (CAA) as amended, and West Virginia 45 CSR30 regulations. However, the Station is required to have a General Permit pursuant to West Virginia 45 CSR13 regulations. The Station currently operates under a Class II General Permit G35-A053, issued on May 10, 2011, with an effective date of May 10, 2011.

#### 1.2 PROJECT OVERVIEW

Dominion is submitting an Application for a Class II General Permit G35-A, to the West Virginia Department of Environmental Protection (WVDEP) for a proposed modification to the Station.





Specifically, Dominion is proposing to remove the existing flare (Emission Point ID: FL-1) that serves as a control device to the glycol dehydration unit, and replace it with a new enclosed flare, which will also serve as an air pollution control device for the existing glycol dehydration unit.

Although 45 CSR§13-4.2(b) identifies a change in control equipment as a Class II administrative update, "flares" meet the 45 CSR§6-2 definition of "incinerator". Because the proposed enclosed flare meets the West Virginia definition of incinerator, the replacement of the control device (i.e., flare) is considered a minor modification. Therefore, in accordance with 45 CSR§13-5, a Class II General Permit application must be submitted to WVDEP for review. This interpretation was confirmed on March 28, 2014 during a phone call with Beverly McKeone of the WVDEP. Therefore, Dominion is submitting this Application for a G35-A General Permit for the proposed project change.

Dominion plans to begin construction upon issuance of this permit (anticipated March, 2015). This Application includes the requisite WVDEP Application form, supporting Application attachments, supporting narrative, and the applicable Application fees.

#### 1.3 APPLICATION ORGANIZATION

This Application is organized in a report format and includes the following sections and appendices:

Section 1 - Introduction

Section 2 - Process Description and Proposed Changes

Section 3 - Emissions Inventory

Section 4 – Regulatory Analysis

Section 5 - Summary of Application Forms and Supporting Information

Appendix A - Application Forms and Attachments

Appendix B – GRI-GLYCalc Emission Summary and Wet Gas Analysis

Appendix C - Flare Design Evaluation



#### 2. PROCESS DESCRIPTION AND PROPOSED CHANGES

The Big Isaac Compressor Station is a natural gas compressor station used to compress gas for Dominion's pipeline system in West Virginia. The Station transports natural gas to a natural gas processing plant while serving the purpose of pumping natural gas from production and gathering lines to a Dominion pipeline. The Station operates under General Permit G35-A053, which was issued May 10, 2011. As part of operations at the Station, Dominion utilizes a glycol dehydration unit. The purpose of the glycol dehydration unit is to remove water and impurities from the inlet natural gas stream. Water is removed from the rich natural gas stream via physical absorption while it flows countercurrent to circulating triethylene glycol (TEG) in a contactor. The rich TEG is sent to a flash tank to reduce volatile hydrocarbons. Vapors from the flash tank are primarily vented back to station suction and reclaimed. Vapors from the reboiler pass through a still column that is controlled by the existing flare referenced as Emission Point ID: FL-1.

Dominion proposes to replace the control device (i.e., flare) for the dehydration unit with a new enclosed flare. For the purposes of this Application, the new enclosed flare will be referenced as Emission Point ID FL-2. As part of the control device replacement, a blow-case will be installed between the still column and enclosed flare on the glycol dehydration unit. The installation of the blow-case is considered part of the control device installation, as it serves to enhance the efficiency of the enclosed flare. The installation of the blow-case is not considered a modification of the glycol dehydration unit. The glycol dehydration unit will not be debottlenecked as a result of the proposed project.

The Emissions Unit Table for the changes associated with this modification is shown in Table 2-1.



Table 2-1
<b>Emission Units Table</b>
<b>Dominion Transportation – Big Isaac Mountain Station</b>

Emission Unit ID	Emission Point ID	Emission Unit Description	Year Installed/ Modified	Design Capacity	Type of Change	Control Device
FL-1	FL-1	Glycol Dehydration Flare	2011	21.0 scf/m	Removal	N/A
FL-2	FL-2	Glycol Dehydration Unit Enclosed Flare, Questor Q50 (95% control efficiency)	2015	22.8 scf/m	New	N/A

The existing flare (Emission Point IDs: FL-1) at the Station is proposed to be replaced by a new Questor Technologies Inc. (Questor) Q50 enclosed flare, referenced within the Application as Emission Point ID FL-2. The new Questor Q50 enclosed flare will operate with a 95% control efficiency. The changes in emissions of criteria pollutants, greenhouse gases (GHG), and HAPs as a result of this project are discussed in Section 3. Emissions of lead (Pb) are insignificant from this source and are not considered further.



#### 3. EMISSIONS INVENTORY

Dominion proposes to replace the existing control device (i.e., flare) with a new control device (i.e., enclosed flare) for the glycol dehydration unit at the Station. For the purposes of this project, emissions were calculated for applicable NSR regulated pollutants except Pb. These pollutants include particulate matter (PM), volatile organic compounds (VOC), nitrogen oxides (NO<sub>X</sub>), carbon monoxide (CO), sulfur dioxide (SO<sub>2</sub>), GHG, and HAPs. Emissions of PM account for both condensable PM and filterable PM, where filterable PM is all PM less than or equal to 30 microns in diameter according the WVDEP Division of Air Quality Guidance for Pollutant Reporting. PM is conservatively assumed to be equivalent to particulate matter less than 10 microns in diameter (PM<sub>10</sub>) and particulate matter less than 2.5 microns in diameter (PM<sub>2.5</sub>).

The proposed replacement control device is a Questor Q50 enclosed flare. A summary of the potential to emit (PTE) of NSR regulated pollutants from the new enclosed flare and the pilot flame is included in Table 3-1. The potential emissions of NOx, CO, and SO<sub>2</sub> are based on vendor guarantees (see Attachment G, located in Appendix A, for the Questor vendor information sheets) which account for emissions associated with the combustion of natural gas and waste gas. The potential emissions of VOC and HAP were calculated using GRI-GLYCalc Version 4.0 with an updated gas analysis, a maximum stripping gas flowrate of 6.9 standard cubic feet per minute (scfm), and natural gas emission factors from AP-42 (Chapter 1.4, Table 1.4-2, 07/98) for VOC and total organic compounds (TOC). The use of stripping gas lowers the partial pressure of the water in the glycol solution, thus increasing the glycol concentration. The GRI-GLYCalc Version 4.0 model was used to calculate the VOC and HAP emissions from the combustion of natural gas from the pilot. The TOC emission factor for natural gas combustion was conservatively used to estimate total HAP emissions from natural gas.

Table 3-1
Dominion Transportation - Big Isaac Compressor Station
Project Related Potential Emissions Summary

		Emissio	on Points	
<b>Regulated Pollutant</b>	RSV-1 (Contr	olled by FL-2)	FL-2	(New)
	(lb/hr)	(tons/yr)	(lb/hr)	(tons/yr)
Mary and Mary Superior	Cr	iteria Pollutants	A DESTRUCTION OF	
PM <sup>(a)</sup>	-	-	0.01	0.05
VOC <sup>(b)</sup>	2.17	9.55	-	
NO <sub>X</sub> <sup>(c)</sup>	~	-	0.07	0.32
CO <sup>(c)</sup>	-		0.06	0.27
SO <sub>2</sub> <sup>(c)</sup>	-	•	0.00	0.00
	Greenh	ouse Gas Pollutants <sup>(d)</sup>	the state of the second	and the second
CO <sub>2</sub> <sup>(e)</sup>	-	-	77.63	340.95
CH4 <sup>(f)</sup>	-	-	0.22	0.97
N <sub>2</sub> O <sup>(g)</sup>	-		8.84E-04	3.88E-03
CO <sub>2</sub> e <sup>(h)</sup>	-	-	83.40	366.29
	Hazar	dous Air Pollutants		2002.000
Total HAP <sup>(b)</sup>	0.24	I.07	-	-

<sup>(a)</sup>Potential emissions of PM include PTE from the combustion of natural gas from the pilot flame and the supplemental natural gas stream, calculated based on the AP-42, Chapter 1.4, Table 1.4-2 emission factor for PM (Total). PM emissions also include PTE from enclosed flare's combustion of emissions from the dehydration still vent and waste fuel gas, calculated based on the AP-42, Chapter 13.5, Table 13.5-1 emission factor for soot, assuming a lightly smoking flare (40  $\mu$ g/L). According to the May 2011 Emission Estimation Protocol for Petrolcum Refineries, approved by the U.S. EPA on March 28, 2011, 40  $\mu$ g/L is equivalent to 0.027 lb/MMBtu. PM is conservatively assumed to be equivalent to all filterable PM including PM<sub>10</sub> and PM<sub>25</sub>, and condensable fractions.

(b) Potential emissions of VOC and HAP include PTE from the pilot flame's natural gas combustion, calculated using AP-42 Chapter 1.4, Table 1.4-2 emissions factors for VOC and TOC, and PTE from enclosed flare's combustion of emissions from the dehydration still vent and fuel gas, calculated using GRI-GLYCalc Version 4.0 and an updated gas analysis. The dehydration still vent VOC and HAP emissions represent the sum of controlled regenerator emissions and flash tank off gas emissions generated using GRI-GLYCalc 4.0 with the incorporation of a 20% safety factor. GRI-GLYCalc summaries are included in Appendix B of the Application.

(e)Potential emissions of NO<sub>X</sub>, CO, and SO<sub>2</sub> are based on vendor specifications, maximum flowrate = 32.88 Mscf/day (22.8 scf/min); waste to fuel gas ratio of 1:0.2.

<sup>(d)</sup>Potential emissions of greenhouse gases are calculated from the combustion of natural gas from the pilot flame, the supplemental natural gas stream, and the waste gas in the enclosed flare. Emissions from the supplemental natural gas fuel and the pilot flame natural gas were calculated using a fuel flowrate of 10,000 scf/day and a pilot flame flowrate of 1,200 scf/day to the enclosed flare. Greenhouse gas pollutant emission factors for the combustion of natural gas were obtained from 40 CFR Part 98, Subpart C. The emissions from the combustion of waste gas use the methodologies outlined below:

<sup>(c)</sup>CO<sub>2</sub> is calculated assuming emissions from both natural gas and waste gas streams in metric tons/year,

calculated according to 40 CFR 98 Equation Y-1a, where:

$$CO_2 = 0.98 \times 0.001 \times \left( \sum_{p=1}^{n} \left[ \frac{44}{12} \times (Flare)_p \times \frac{(MW)_p}{MVC} \times (CC)_p \right] \right)$$

<sup>(1)</sup>CH<sub>4</sub> is in metric tons/year, calculated according to 40 CFR 98 Equation Y-4, where:

$$CH_4 = \left(CO_2 \times \frac{EmF_{CH4}}{EmF}\right) + CO_2 \times \frac{0.02}{0.98} \times \frac{16}{44} \times f_{CH4}$$

<sup>(8)</sup>N<sub>2</sub>O is in metric tons/year, calculated according to 40 CFR 98 Equation Y-5, where:

$$N_{2}O = \left(CO_{2} \times \frac{EmF_{N2O}}{EmF}\right) \qquad (Eq. Y-5)$$

<sup>(h)</sup>CO<sub>2</sub>e is carbon dioxide equivalent in metric tons/year, calculated according to 40 CFR 98 Equation A-1, where:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

Table A-1: Global Wa	rming Potentials
Pollulant	GWP (100 year)
CO2	I
CH <sub>4</sub>	25
N-O	298

Flare p = volume flare gas combusted = ~23 acfm MW = molecular weight flare gas = 21 kg/kg-mol.

MVC = molar conversion factor of 849.5 scf/kg-mol at 68°F

CC = carbon concentration of flare gas = 7.87%.

0.98 = combustion efficiency of flare (used 0.95 for 95% efficiency)

 $\mathsf{EmF}_{\mathsf{CH4}}=\mathsf{Default}\;\mathsf{CH_4}\;\mathsf{emission}\;\mathsf{factor}\;\mathsf{for}\;"\mathsf{Fuel}\;\mathsf{Gas"}\;\mathsf{from}\;\mathsf{Table}\;\mathsf{C-2}$ 

 $EmF = default CO_2 emission factor for flare gas of 60 kg/CO_2/MMBtu.$ 

 $CO_2$  = emission rate of  $CO_2$  from flared gas in metric tons/year.

 $f_{CH4}$  = default weight fraction of carbon in flare gas of 0.4

0 98 = combustion efficiency of flare (used 0 95 for 95% efficiency)

 $\begin{array}{l} CO_2 = emission \ rate \ of \ CO_2 \ from \ flared \ gas \ in \ metric \ tons/year. \\ EmF_{N2O} = Default \ N_2O \ emission \ factor \ for \ fruel \ Gas" \ from \\ Table \ C-2 \\ EmF = default \ CO_2 \ emission \ factor \ for \ flare \ gas \ of \ 60 \\ kg/CO_2/MMBtu. \end{array}$ 

 $GHG_i$  = mass emissions of each greenhouse gas listed in Table A-1, metric tons/year.  $GWP_i$  = global warming potential for each greenhouse gas from

Table A-1. n = number of greenhouse gases emitted.

Table 3-2
Dominion Transportation - Big Isaac Compressor Station
Project Related Changes in Potential Emissions Summary

Regulated Pollutant	0	Potential E (tons/yr) <sup>(a)</sup>		0	t Related Positions	224 32	Change i	n Potential I (tons/yr) <sup>(c)</sup>	Emissions	Summary of Changes in Potential Emissions <sup>(d)</sup>
	RBV-1	RSV-1	FL-1	RBV-1	RSV-1	FL-2	RBV-1	RSV-1	FL-2	
	11111			C	riteria Pollu	itants	1 55		11.03/20	REAK LINE REAL
PM	< 0.01	-	-	< 0.01	-	0.05	< 0.01		0.05	0.05
VOC	0.17	3.97	-	0.17	9.55	-	0.00	5.58	-	5.58
NO <sub>X</sub>	0.22	-	0.22	0.22	-	0.32	0.00	-	0.1	0.10
СО	0.18	-	0.70	0.18	-	0.27	0.00	-	0.00	0.00
SO <sub>2</sub>	< 0.01	-	-	< 0.01	-	-	< 0.01	Ξ.	-	0.00
				Green	house Gas	Pollutants				
CO <sub>2</sub> e	239.17	-	2,485.66	239.17	-	366.29	0.00	-	0.00	0.00
				Haza	rdous Air P	ollutants				
Total HAP	< 0.01	0.71	-	< 0.01	1.07	-	< 0.01	0.36		0.36

<sup>(a)</sup> As reported in Attachment I of the G35-A General Permit application submitted to the West Virginia Department of Environmental Protection (WVDEP) on April 6, 2011. <sup>(b)</sup> As calculated in Table 3-1 of this G35-A General Permit application.

<sup>(c)</sup> Change in Potential Emissions = ([Project Related Potential Emissions] - [Existing Potential Emissions]).

<sup>(d)</sup> Summary of Changes in Potential Emissions represents the increase in potential emissions from the facility as a result of the proposed project.



A summary of the GRI-GLYCalc inputs and results are included in Appendix B. Potential emissions of PM include emissions from the combustion of natural gas used for the pilot flame and the supplemental natural gas stream (calculated using the emission factor from AP-42, Chapter 1.4, Table 1.4-2, 07/98 for PM-Total). The potential emissions of PM also include emissions from the combustion of waste gas in the enclosed flare (calculated using AP-42 Chapter 13.5, Table 13.5-1, 09/91 emission factors for soot, conservatively assuming a lightly smoking flare).

Potential emissions of GHG from the new enclosed flare include emissions from the combustion of waste gas from the glycol dehydration unit and the combustion of natural gas used for the pilot flame and the supplemental natural gas inlet stream. GHG were calculated on a carbon dioxide equivalent (CO<sub>2</sub>e) basis by adding the potential emissions of carbon dioxide (CO<sub>2</sub>) with potential emissions of nitrous oxide (N<sub>2</sub>O) and methane (CH<sub>4</sub>), using the emission factors, global warming potential (GWP), and methodology obtained from 40 CFR 98, Subparts C and Y. GHG emissions from the combustion of the glycol dehydration unit's waste gas were calculated pursuant to 40 CFR Part 98, Subpart Y (Petroleum Refineries). This method was used rather than 40 CFR Part 98, Subpart W (Petroleum and Natural Gas Systems) because Subpart Y more appropriately estimates GHG emissions based on the specifications of glycol dehydration units. GHG emissions from the combustion of natural gas used for the pilot flame and the supplemental natural gas inlet stream were calculated based on emission factors obtained from 40 CFR Part 98, Subpart 98, Subpart 2, Tables C-1 and C-2, and the maximum natural gas flowrate supplied to the enclosed flare.

The PTE of the new enclosed flare was calculated by assuming 8,760 operating hours per year, and a maximum volumetric flowrate of 22.8 standard cubic feet per minute (scf/min), based on the design capacity of the new Questor Q50 enclosed flare. A summary of project related changes in emissions can be found in Attachment G, located within Appendix A. The summary of Facility-wide emissions following the replacement of the existing control device (i.e., flare) can also be found in Attachment G, located in Appendix A.



#### 4. **REGULATORY ANALYSIS**

Dominion has reviewed the Federal and State of West Virginia air quality regulations for potentially applicable requirements that could impact the proposed project. The following sections address only those air regulations that could apply to the proposed project.

#### 4.1 FEDERAL AIR QUALITY REGULATIONS

For the purpose of this application, potentially applicable Federal regulations include the following:

- New Source Performance Standards (NSPS)
- National Emission Standards for Hazardous Air Pollutants (NESHAP)
- Compliance Assurance Monitoring (CAM)
- New Source Review (NSR)

A discussion of each specific Federal requirement is presented in the following subsections.

#### 4.1.1 New Source Performance Standards (NSPS)

The United States Environmental Protection Agency (U.S. EPA) has promulgated standards of performance for new, modified, or reconstructed sources of air pollution at 40 CFR Part 60, referred to as New Source Performance Standards (NSPS). Neither the enclosed flare nor the glycol dehydration unit is subject to an NSPS regulation. The proposed project will not impact the applicability of existing NSPS, and/or the Station's ability to comply with the applicable requirements.

#### 4.1.2 National Emission Standards for Hazardous Air Pollutants (NESHAP)

U.S. EPA has promulgated National Emission Standards for Hazardous Air Pollutants (NESHAP) at 40 CFR Part 63. Several existing emission units at the Station are already subject to a NESHAP. The proposed project will not impact the applicability of any NESHAP, or the Station's ability to comply with previously applicable requirements. The following Part 63 Subparts potentially apply to the proposed project:

<u>Subpart A</u> – General Provisions



- <u>Subpart HH</u> NESHAP for Oil and Natural Gas Production Facilities
- <u>Subpart HHH</u> NESHAP for Natural Gas Transmission and Storage Facilities

#### 4.1.2.1 40 CFR Part 63, Subpart A – General Provisions

Pursuant to the Clean Air Act Amendments of 1990, process-specific NESHAPs are promulgated at 40 CFR Part 63. NESHAPs promulgated under 40 CFR Part 63, also referred to as Maximum Achievable Control Technology (MACT) standards, apply to identified source categories that are considered area sources or major sources of HAPs. As previously mentioned in Section 1.1, the potential emissions of HAPs from the Station are less than the major source thresholds. Therefore, the Station qualifies as an area source of HAPs as defined in §63.2. As an area source of HAPs, the glycol dehydration unit at the Station is potentially subject to MACT standards codified at 40 CFR Part 63. Note that the existing flare serving as a control device for the glycol dehydration unit, and replacement enclosed flare are subject to the control device and work practice requirements specified in Condition No. 10.1.4 of General Permit 35-A053, which are based on provisions in 40 CFR §63.11 (Subpart A).

#### 4.1.2.2 40 CFR Part 63, Subpart HH – NESHAP for Oil and Natural Gas Production Facilities

The Station is subject to 40 CFR Part 63, Subpart HH – *National Emission Standards for Hazardous Air Pollutants from Oil and Natural Gas Production Facilities* (Subpart HH) because the Station transports natural gas to a natural gas process plant. The Station is subject to the area source requirements, and the only affected source is the Station's glycol dehydration unit. The glycol dehydration unit at the Station meets the definition of a large glycol dehydration unit because its actual annual gas flowrate is greater than 85 thousand standard cubic meters per day (Mm<sup>3</sup>/day), and its uncontrolled benzene emissions are greater than 0.90 megagrams per year (Mg/yr), or 1 tpy. The Station is not located within an urbanized area plus offset (UA plus offset) and urban cluster (UC) boundary. A map depicting the location determination is included in Attachment F.

The Station's glycol dehydration unit actual average benzene emissions (i.e., controlled emissions) are less than 0.90 Mg/yr (1 tpy), as determined in accordance with §63.772(b)(2)(i). Therefore, the Station's glycol dehydration unit meets the exemption criteria as specified by



§63.764(e)(ii). Potential actual average benzene emissions following the replacement of the control device will remain less than 0.90 Mg/yr (1 tpy), due to the emissions reductions associated with the federally enforceable controls (i.e., replacement enclosed flare) in place per §63.772(b)(2). Because the control device replacement continues to reduce the potential annual potential benzene emissions to less than 0.90 Mg/yr (1 tpy), the dehydration unit will remain exempt from the requirements of §63.764(d)(1)(i) through (iii). Records associated with this determination will be maintained in accordance with §63.774(d)(1). Although the dehydration unit is not subject to control device requirements of 40 CFR 63 Subpart HH or Subpart A, the dehydration unit's control devices (existing flare and replacement enclosed flare) are subject to the control device and work practice requirements specified in §63.11 (Subpart A), as required per Condition No. 10.1.4 of General Permit 35-A053.

# 4.1.2.3 Condition40 CFR Part 63, Subpart HHH – NESHAP for Natural Gas Transmission and Storage Facilities

The provisions of 40 CFR Part 63, Subpart HHH apply to glycol dehydration units located at natural gas transmission and storage facilities that transport or store natural gas prior to entering the pipeline to a local distribution company or to a final end user. Because the Station is a natural gas production facility, HHH does not apply.

#### 4.1.3 Compliance Assurance Monitoring (CAM)

U.S. EPA promulgated the Compliance Assurance Monitoring (CAM) rule at 40 CFR Part 64 on October 22, 1997 with an effective date of November 21, 1997. U.S. EPA developed the regulation as a means for providing reasonable assurance that an emissions unit is in continuous compliance with applicable requirements for affected units located at major stationary sources subject to Title V permitting. According to 40 CFR §64.2(a), a unit located at a nonmajor source that is not required to obtain Title V permit, is exempt from CAM. Therefore, the Station is not subject to CAM requirements.



#### 4.1.4 New Source Review (NSR)

U.S. EPA has approved West Virginia's NSR regulations through their incorporation into the West Virginia State Implementation Plan (SIP). The state-specific NSR regulations are codified in West Virginia 45 CSR§14 and 19.

#### 4.1.4.1 Prevention of Significant Deterioration (PSD)

The Prevention of Significant Deterioration (PSD) regulations ensure that major new sources and major modifications to existing sources will not result in the significant deterioration of air quality in areas designated by U.S. EPA as in attainment of National Ambient Air Quality Standards (NAAQS). Because the replacement of the existing control device (i.e. replacement enclosed flare) is not a major modification and since the Station is not a major source under the PSD rules, PSD does not apply.

#### 4.1.4.2 Nonattainment New Source Review (NNSR)

The NNSR regulations ensure that major new sources and major modifications to existing sources located in areas of nonattainment of NAAQS will not adversely impact the area's progress toward achieving NAAQS. Because the change is not a major source when considered alone and as the Station is not a major source under the PSD rules, the NNSR rules do not apply.

#### 4.2 STATE OF WEST VIRGINIA REQUIREMENTS

The proposed project is potentially subject to the following West Virginia air quality regulations as codified in Title 45 – Division of Air Quality Code. It should be noted that none of the existing Title 45 regulations that currently apply to the Station will be impacted by the proposed project.

- 45 CSR6 To Prevent and Control Air Pollution from Combustion of Refuse
- 45 CSR10 To Prevent and Control Air Pollution from the Emission of Sulfur Oxides
- 45 CSR13 Permits for Construction, Modification, Relocation, and Operation of Stationary Sources of Air Pollutants
- 45 CSR30 Requirements of Operating Permits
- 45 CSR30A Deferral of Nonmajor and Area Sources from Permitting Requirements



45 CSR34 – Emission Standards for Hazardous Air Pollutants

#### 4.2.1 45 CSR6 – To Prevent and Control Air Pollution from Combustion of Refuse

The provisions of this rule establish emission standards for PM and requirements for activities involving incineration of refuse which are not subject to, or are exempted from regulation under a federal counterpart for specific combustion sources. The proposed control device (i.e., enclosed flare) for the glycol dehydration unit at the Station meets the definition of an "incinerator" in 45 CSR§6-2, and therefore is subject to the 45 CSR6 regulations. The monitoring requirements, testing requirements, recordkeeping requirements, and reporting requirements of this rule therefore apply.

Based on 45 CSR§6-4, the allowable PM emissions for the flare are calculated using the following formula:

$$PM_{allowable}\left(\frac{lb}{hr}\right) = Incinerator \ Capacity \left(\frac{tons}{hr}\right) x F$$

Where: F = Factor for determining maximum allowable particulate emissions. For incinerators with a capacity less than 15,000 lb/hr: F = 5.43. *Incinerator Capacity* = design capacity of the flare (estimated total flow rate to the flare, including materials to be burned, carrier gases, auxiliary fuel, etc.).

The allowable PM limit calculation is provided below:

$$PM_{allowable} = 106 \frac{lb}{hr} x 5.43 (F factor) x \frac{1 ton}{2000 lb} = 0.29 lb/hr,$$

Based on AP-42, the enclosed flare will comply with the allowable PM emission limit determined in accordance with 45 CSR §6-4.

# 4.2.2 45 CSR10 – To Prevent and Control Air Pollution from the Emission of Sulfur Oxides (SO<sub>x</sub>)

The provisions of this rule regulate emissions of SO<sub>X</sub>. The existing control device (i.e., flare) is subject to the applicable emission limits specified in 45 CSR§10-4.1 Standards for Manufacturing Process Source Operations and 45 CSR§10-5.1 Combustion of Refinery or Process Gas Streams. The existing source-specific emission limits will not change as a result of the proposed project. The new enclosed flare is exempt from the testing, monitoring,



recordkeeping, and reporting requirements of 45 CSR§10-8 because it combusts natural gas (CSR§10-10.3).

# 4.2.3 45 CSR13 – Permits for Construction, Modification, Relocation, and Operation of Stationary Sources of Air Pollutants

The provisions of this rule set forth the procedures for stationary source reporting, and the criteria for obtaining a permit to modify a nonmajor stationary source. The proposed project is a modification to a nonmajor source as defined in 45 CSR13, and therefore requires a General Permit.

# 4.2.4 45 CSR30 – Requirements of Operating Permits and 45 CSR30A – Deferral of Nonmajor and Area Sources From Permitting Requirements

The provisions of 45 CSR30A provide for the deferral of nonmajor and area sources from the obligation to obtain a permit under 45 CSR30. 45 CSR30 provides for the establishment of a comprehensive air permitting system consistent with the requirements of Title V of the CAA. As the Station meets the definition of a nonmajor facility and is not a major Title V source for criteria pollutants, the monitoring, recordkeeping, and reporting requirements contained in 45 CSR30 do not apply.

#### 4.2.5 45 CSR34 – Emission Standards for Hazardous Air Pollutants (HAP)

The provisions of this rule incorporate 40 CFR Parts 61 and 63 by reference including any required methods, performance specifications, and all test methods which are approved to flare standards. Exclusions are identified at 45 CSR§34-4. The proposed project does not affect the applicability of 45 CSR34. Therefore, the standards set forth by 40 CFR Part 63, Subpart HH will continue to apply.



# 5. SUMMARY OF APPLICATION FORMS AND SUPPORTING INFORMATION

Dominion is including a check payable to the "West Virginia Department of Environmental Protection – Division of Air Quality" in the amount of \$3,000, as established in 45 CSR§22-3.4(a) and (b), to cover the G-35-A General Permit Application fees (\$500) for applicable sources subject to NESHAP requirements (\$2,500).

The following attachments included as Appendix A provide supporting information for the General Permit G35-A Application:

- Attachment A Business Certificate
- Attachment B Process Description
- Attachment D Process Flow Diagram
- Attachment E Plot Plan
- Attachment F Area Map
- Attachment G Equipment Data Sheets
- Attachment H Air Pollution Control Device Sheets
- Attachment I Emission Calculations
- Attachment J Class I Legal Advertisement
- Attachment L General Permit Registration Application Fee

\*\*Note - There are no Attachments C, H, K, M, N and O for this permit application

### APPENDIX A APPLICATION FORMS AND ATTACHMENTS

		_		
WEST VIRG DEPARTMENT OF ENVIRONM DIVISION OF AIR 601 57 <sup>th</sup> Stree Charleston, WV	IENTAL PROTECTIC QUALITY et, SE 25304		<b>F</b> COI	PLICATION FOR GENERAL PERMIT REGISTRATION NSTRUCT, MODIFY, RELOCATE OR ADMINISTRATIVELY UPDATE
Phone: (304) 926-0475 • v	/ww.dep.wv.gov/daq			IONARY SOURCE OF AIR POLLUTANT
	ASS II ADMINISTE		-	CLASS   ADMINISTRATIVE UPDATE
CHECK WHICH TYPE OF C	SENERAL PERMI	T REGIST	RATIO	N YOU ARE APPLYING FOR:
G10-D – Coal Preparation and Handling				
G20-B – Hot Mix Asphalt			_	-C – Nonmetallic Minerals Processing
G30-D – Natural Gas Compressor Stations				-B – Concrete Batch
G33-A – Spark Ignition Internal Combustion Engine			[_]G60-	-C - Class II Emergency Generator
			G65-	-C – Class I Emergency Generator
G35-A – Natural Gas Compressor Stations (Flar	e/Glycol Dehydratio	on Unit)	_]G70-	-A – Class II Oil and Natural Gas Production Facilit
S	ECTION I. GENE		RMATI	ON
1. Name of applicant (as registered with the WV Secr Dominion Transmission, Inc.				2. Federal Employer ID No. (FEIN): 550629203
Clarksburg, WV 26301         5. If applicant is a subsidiary corporation, please prov	ride the name of pare			n County, West Virginia 26426
6. WV BUSINESS REGISTRATION. Is the applicant			0	VES / Limited Partnership (one page) including any na
change amendments or other B	usiness Registration	Certificate	as Attac	hment A.
<ul> <li>IF NO, provide a copy of the Cert amendments or other Business</li> </ul>			of LLC	/ Registration (one page) including any name cha
s	ECTION II. FACIL		RMATI	ON
7. Type of plant or facility (stationary source) to be co		a. Standard	d Industri	al Classification (SIC) code: 4922
modified, relocated or administratively updated (e.g., o plant, primary crusher, etc.):	coal preparation 8t	b. North Ar	nerican lı	ndustry Classification System (NAICS) code: 4862
Replacement of glycol dehydration unit cont (i.e., flare) with a new control device (i.e., end				
9. DAQ Plant ID No. (for existing facilities only): 017	00000			CSR13 and other General Permit numbers associa existing facilities only): G35-A053

11A. Facility name of primary operating site:	12A. Address of primary operating site:	
······································		
Big Isaac Compressor Station	1 -	Physical:
		CR 28/Coburn Fork Rd. & Raccoon Run Rd. Salem, Harrison County, West Virginia 26426
13A. Does the applicant own, lease, have an op	tion to buy, or otherwise have control of the	proposed site? YES
- IF YES, please explain: The applicant of		
- IF NO, YOU ARE NOT ELIGIBLE FOR A F	PERMIT FOR THIS SOURCE.	
14A. – For <b>Modifications or Administrative</b> nearest state road;	Updates at an existing facility, please provi	de directions to the present location of the facility from
<ul> <li>For Construction or Relocation permits</li> <li>MAP as Attachment F.</li> </ul>	, please provide directions to the proposed	new site location from the nearest state road. Include
Street, and stay left at the fork to continue fork and continue to until CR15 intersect until Raccoon Run Road. The Big Isaac	ie driving south on CR29. At the int s CR28 (Coburn Fork Road). Turn l	ersection of CR 29 and CR15, stay left at the
Street, and stay left at the fork to continu fork and continue to until CR15 intersect until Raccoon Run Road. The Big Isaac Road) and Raccoon Run Road.	ie driving south on CR29. At the int is CR28 (Coburn Fork Road). Turn lo Compressor Station will be on the lo	ersection of CR 29 and CR15, stay left at the eft on CR28 (Coburn Fork Road) and continu eft at the intersection of CR28 (Coburn Fork
Street, and stay left at the fork to continu fork and continue to until CR15 intersect until Raccoon Run Road. The Big Isaac Road) and Raccoon Run Road.	le driving south on CR29. At the int is CR28 (Coburn Fork Road). Turn le Compressor Station will be on the le 16A. County:	ersection of CR 29 and CR15, stay left at the eft on CR28 (Coburn Fork Road) and continu eft at the intersection of CR28 (Coburn Fork 17A. UTM Coordinates:
Street, and stay left at the fork to continue fork and continue to until CR15 intersect until Raccoon Run Road. The Big Isaac Road) and Raccoon Run Road. 15A. Nearest city or town:	ie driving south on CR29. At the int is CR28 (Coburn Fork Road). Turn lo Compressor Station will be on the lo	ersection of CR 29 and CR15, stay left at the eff on CR28 (Coburn Fork Road) and continu eff at the intersection of CR28 (Coburn Fork 17A. UTM Coordinates: Northing (KM): <b>4344.0282</b>
Street, and stay left at the fork to continue fork and continue to until CR15 intersect until Raccoon Run Road. The Big Isaac Road) and Raccoon Run Road. 15A. Nearest city or town:	le driving south on CR29. At the int is CR28 (Coburn Fork Road). Turn le Compressor Station will be on the le 16A. County:	ersection of CR 29 and CR15, stay left at the eft on CR28 (Coburn Fork Road) and continu eft at the intersection of CR28 (Coburn Fork 17A. UTM Coordinates:
Street, and stay left at the fork to continue fork and continue to until CR15 intersect until Raccoon Run Road. The Big Isaac Road) and Raccoon Run Road. 15A. Nearest city or town: Salem 18A. Eriefly describe the proposed new operatio	n or change (s) to the facility:	ersection of CR 29 and CR15, stay left at the eff on CR28 (Coburn Fork Road) and continu- eff at the intersection of CR28 (Coburn Fork 17A. UTM Coordinates: Northing (KM): <b>4344.0282</b> Easting (KM): <b>538.3356</b> Zone: <b>17</b> 19A. Latitude & Longitude Coordinates (NAD83
Street, and stay left at the fork to continue fork and continue to until CR15 intersect until Raccoon Run Road. The Big Isaac Road) and Raccoon Run Road. 15A. Nearest city or town: Salem 18A. Briefly describe the proposed new operatio Dominion Transmission, Inc. is proposin flare to replace the existing flare used as	e driving south on CR29. At the int is CR28 (Coburn Fork Road). Turn le Compressor Station will be on the le 16A. County: Doddridge County n or change (s) to the facility: in or change (s) to the facility: in the construct one (1) new enclosed is control devices on the glycol	ersection of CR 29 and CR15, stay left at the eff on CR28 (Coburn Fork Road) and continu- eff at the intersection of CR28 (Coburn Fork 17A. UTM Coordinates: Northing (KM): <b>4344.0282</b> Easting (KM): <b>538.3356</b> Zone: <b>17</b> 19A. Latitude & Longitude Coordinates (NAD83
Street, and stay left at the fork to continue fork and continue to until CR15 intersect until Raccoon Run Road. The Big Isaac Road) and Raccoon Run Road. 15A. Nearest city or town: Salem 18A. Briefly describe the proposed new operatio Dominion Transmission, Inc. is proposin flare to replace the existing flare used as	e driving south on CR29. At the int is CR28 (Coburn Fork Road). Turn le Compressor Station will be on the le 16A. County: Doddridge County n or change (s) to the facility: in or change (s) to the facility: in the construct one (1) new enclosed is control devices on the glycol	ersection of CR 29 and CR15, stay left at the eff on CR28 (Coburn Fork Road) and continu- eff at the intersection of CR28 (Coburn Fork 17A. UTM Coordinates: Northing (KM): <b>4344.0282</b> Easting (KM): <b>538.3356</b> Zone: <b>17</b> 19A. Latitude & Longitude Coordinates (NAD8: Decimal Degrees to 5 digits):
Street, and stay left at the fork to continue fork and continue to until CR15 intersect until Raccoon Run Road. The Big Isaac Road) and Raccoon Run Road. 15A. Nearest city or town: Salem 18A. Briefly describe the proposed new operatio Dominion Transmission, Inc. is proposin flare to replace the existing flare used as dehydration system located at the Big Is	e driving south on CR29. At the int is CR28 (Coburn Fork Road). Turn le Compressor Station will be on the le 16A. County: Doddridge County in or change (s) to the facility: in or change (s) to the facility: in or change (s) to the facility: control devices on the glycol aac Compressor Station.	ersection of CR 29 and CR15, stay left at the eff on CR28 (Coburn Fork Road) and continu- eff at the intersection of CR28 (Coburn Fork 17A. UTM Coordinates: Northing (KM): 4344.0282 Easting (KM): 538.3356 Zone: 17 19A. Latitude & Longitude Coordinates (NAD83 Decimal Degrees to 5 digits): Latitude: 39.2470 Longitude: -80.5563
Street, and stay left at the fork to continue fork and continue to until CR15 intersect until Raccoon Run Road. The Big Isaac Road) and Raccoon Run Road. 15A. Nearest city or town: Salem 18A. Briefly describe the proposed new operatio Dominion Transmission, Inc. is proposin flare to replace the existing flare used as dehydration system located at the Big Is B: 1 <sup>st</sup> ALTERNATE OPERAT	e driving south on CR29. At the int is CR28 (Coburn Fork Road). Turn le Compressor Station will be on the le 16A. County: Doddridge County n or change (s) to the facility: in or change (s) to the facility: in the construct one (1) new enclosed is control devices on the glycol	ersection of CR 29 and CR15, stay left at the eff on CR28 (Coburn Fork Road) and continu- eff at the intersection of CR28 (Coburn Fork 17A. UTM Coordinates: Northing (KM): 4344.0282 Easting (KM): 538.3356 Zone: 17 19A. Latitude & Longitude Coordinates (NAD8: Decimal Degrees to 5 digits): Latitude: 39.2470 Longitude: -80.5563
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13B. Does the applicant own, lease, have an option to buy, or otherwise have control of the proposed site? **N/A** 

- IF YES, please explain: N/A
- IF NO, YOU ARE NOT ELIGIBLE FOR A PERMIT FOR THIS SOURCE.

14B. –	For Modifications or Administrative Updates at an existing facility, please provide directions to the present location of the facility from the
	nearest state road;
_	For Construction or Relocation permits, please provide directions to the proposed new site location from the nearest state road. Include a

For Construction or Relocation permits, please provide directions to the proposed new site location from the nearest state road. Include a MAP as Attachment F.

N/A

	15B. Nearest city or town:	16B. County:	17B. UTM Coordinates:
<u>_</u>	N/A	N/A	Northing (KM): <b>N/A</b> Easting (KM): <b>N/A</b>
			Zone: N/A
	18B. Briefly describe the proposed new operation <b>N/A</b>	19B. Latitude & Longitude Coordinates (NAD83, Decimal Degrees to 5 digits):	
			Latitude: N/A
			Longitude: N/A

C: 2 <sup>ND</sup> ALTERNATE OPERATING SITE INFORMATION (only available for G20, G40, & G50 General Permits):				
11C. Name of 2 <sup>nd</sup> alternate operating site: <i>N/A</i>	12C. Address of 2 Mailing: <b>N/A</b> Physical: <b>N/A</b>	2 <sup>nd</sup> alternate operating site:		
13C. Does the applicant own, lease, have an optic	on to buy, or otherw	ise have control of the propose	ed site? N/A	
<ul> <li>IF YES, please explain: N/A</li> </ul>				
- IF NO, YOU ARE NOT ELIGIBLE FOR A PE	RMIT FOR THIS S	OURCE		
14C. – For Modifications or Administrative U nearest state road;	pdates at an existir	ng facility, please provide direct	tions to the present location of the facility from the	
<ul> <li>For Construction or Relocation permits, MAP as Attachment F.</li> <li>N/A</li> </ul>	please provide dire	ctions to the proposed new site	e location from the nearest state road. Include a	
15C. Nearest city or town:	16C. County:		17C. UTM Coordinates:	
N/A	N/A		Northing (KM): <b>N/A</b> Easting (KM): <b>N/A</b>	
			Zone: N/A	
18C. Briefly describe the proposed new operation <b>N/A</b>				
MA			Latitude: N/A	
			Longitude: N/A	
		21. Date of anticipated Start-	up if registration is granted:	
20. Provide the date of anticipated installation or change:		N/A		
N/A				
If this is an After-The-Fact permit application, p upon which the proposed change did happen: :	provide the date			
_ N/A				
22. Provide maximum projected <b>Operating Scheo</b> other than 24/7/52 may result in a restriction to the			if other than 8760 hours/year. (Note: anything	
Hours per day <b>N/A</b> Days per week <b>N/A</b> W	/eeks per year <b>N/A</b>	Percentage of operation N	/A	

#### SECTION III. ATTACHMENTS AND SUPPORTING DOCUMENTS

24. Include a Table of Contents as the first page of your application package.				
All of the required forms and additional information can be found under the Permitting Section (General Permits) of DAQ's website, or requested by phone.				
25. Please check all attachments included with this permit application. Please refer to the appropriate reference document for an explanation of the attachments listed below.				
	ATTACHMENT A : CURRENT BUSINESS CERTIFICATE			
	ATTACHMENT B: PROCESS DESCRIPTION			
	ATTACHMENT C: DESCRIPTION OF FUGITIVE EMISSIONS			
	ATTACHMENT D: PROCESS FLOW DIAGRAM			
	ATTACHMENT E: PLOT PLAN			
	ATTACHMENT F: AREA MAP			
	XATTACHMENT G: EQUIPMENT DATA SHEETS AND REGISTRATION SECTION APPLICABILITY FORM			
	ATTACHMENT H: AIR POLLUTION CONTROL DEVICE SHEETS			
	ATTACHMENT I: EMISSIONS CALCULATIONS			
	⊠ATTACHMENT J: CLASS I LEGAL ADVERTISEMENT			
	ATTACHMENT K: ELECTRONIC SUBMITTAL			
	XATTACHMENT L: GENERAL PERMIT REGISTRATION APPLICATION FEE			
	ATTACHMENT M: SITING CRITERIA WAIVER			
	ATTACHMENT N: MATERIAL SAFETY DATA SHEETS (MSDS)			
	ATTACHMENT O: EMISSIONS SUMMARY SHEETS			
	OTHER SUPPORTING DOCUMENTATION NOT DESCRIBED ABOVE (Equipment Drawings, Aggregation Discussion, etc.)			
the addre Virginia A	ail an original and two copies of the complete General Permit Registration Application with the signature(s) to the DAQ Permitting Section, at ss shown on the front page of this application. Please DO NOT fax permit applications. For questions regarding applications or West ir Pollution Rules and Regulations, please refer to the website shown on the front page of the application or call the phone number also on the front page of the application.			

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	SECTION IV. CERTIFICATION	
Presid structu Liabilit mainte notifica Repres	ent, Secretary, Treasurer, General Partner, General Manager, re. A business may certify an Authorized Representative who of Company, Association, Joint Venture or Sole Proprietorship. nance, general correspondence, Emission Inventory, Certified tions must be signed by a Responsible Official or an Authorized	Emission Statement, compliance certifications and all required ad Representative. If a business wishes to certify an Authorized the appropriate names and signatures entered. Any administra
	FOR A CORPORATION (domestic or foreign)           I certify that I am a President, Vice President, Secr           corporation	etary, Treasurer or in charge of a principal business function of
	FOR A PARTNERSHIP	
	FOR A LIMITED LIABILITY COMPANY I certify that I am a General Partner or General Ma	nager
	FOR AN ASSOCIATION	Board of Directors
	FOR A JOINT VENTURE	General Manager
	FOR A SOLE PROPRIETORSHIP	
is an A Liabilit	Company, Association Joint Venture or Sole Proprietorship) a	he interest of the business (e.g., Corporation, Partnership, Limit and may obligate and legally bind the business. If the business otify the Director of the Office of Air Quality immediately, and/or,
hereto	y certify that all information contained in this General Permit R is, to the best of my knowledge, true, accurate and complete, a hensive information possible	egistration Application and any supporting documents appended and that all reasonable efforts have been made to provide the m
Signature	the the l	12-19-14
(please use blue ink)	Responsible Official	Date
Name & Title_	Brian Sheppard, Vice President, Pipeline Operat	ions
(please print or type)		
Signature		0.45
N	Authorized Representative (if applicable)	Date
Applicant's Nar	ne Dominion Transmission, Inc.	
Phone & Fax _		<b>304-627-3323</b>
Email	Brian.C.Sheppard@dom.com	, uA

### ATTACHMENT A BUSINESS CERTIFICATE

# WEST VIRGINIA STATE TAX DEPARTMENT BUSINESS REGISTRATION CERTIFICATE

ISSUED TO: DOMINION TRANSMISSION INC 445 W MAIN ST CLARKSBURG, WV 26301-2843

#### BUSINESS REGISTRATION ACCOUNT NUMBER:

1038-3470

This certificate is issued on: 06/8/2011

This certificate is issued by the West Virginia State Tax Commissioner in accordance with Chapter 11, Article 12, of the West Virginia Code

The person or organization identified on this certificate is registered to conduct business in the State of West Virginia at the location above.

This certificate is not transferrable and must be displayed at the location for which issued. This certificate shall be permanent until cessation of the business for which the certificate of registration was granted or until it is suspended, revoked or cancelled by the Tax Commissioner.

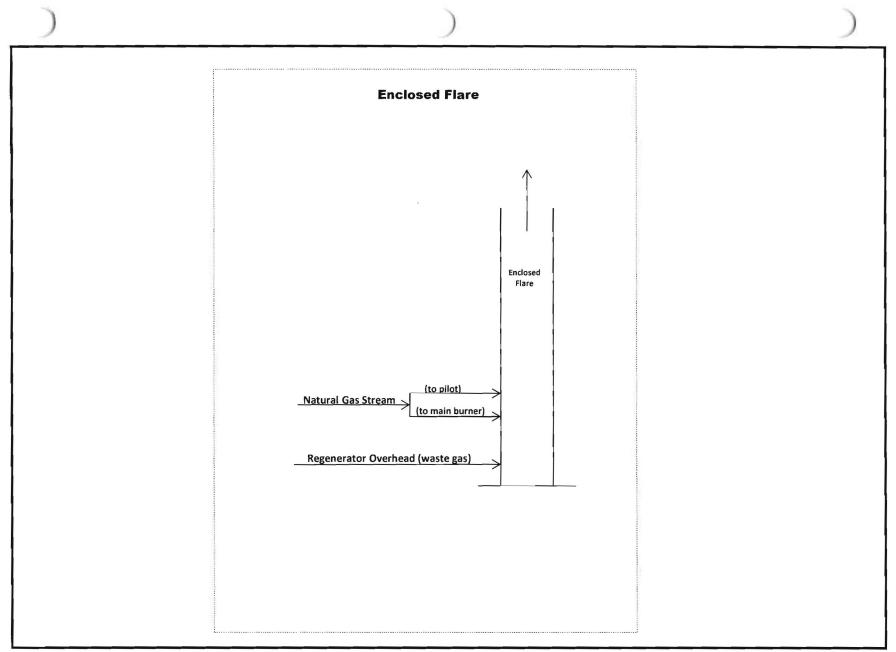
Change in name or change of location shall be considered a cessation of the business and a new certificate shall be required.

TRAVELING/STREET VENDORS: Must carry a copy of this certificate in every vehicle operated by them. CONTRACTORS, DRILLING OPERATORS, TIMBER/LOGGING OPERATIONS: Must have a copy of this certificate displayed at every job site within West Virginia.

alL006 v.4 L0228957312

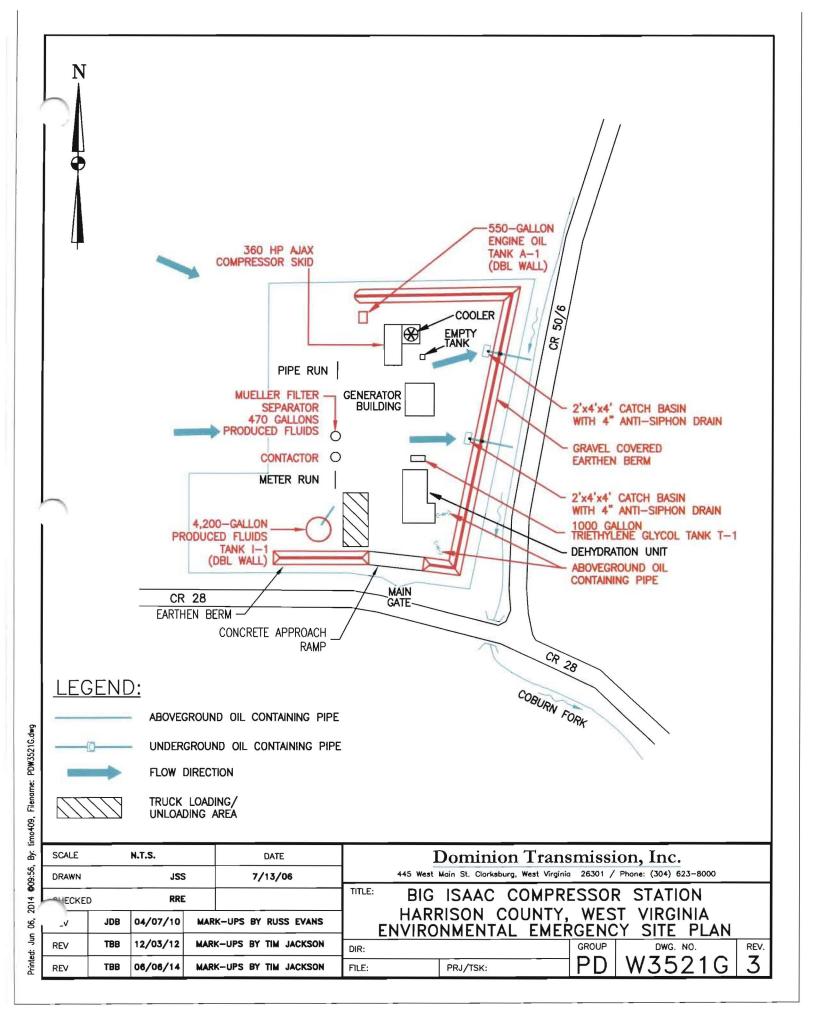
## ATTACHMENT B PROCESS DESCRIPTION (IN SECTION 2 OF TEXT)

### ATTACHMENT D PROCESS FLOW DIAGRAM

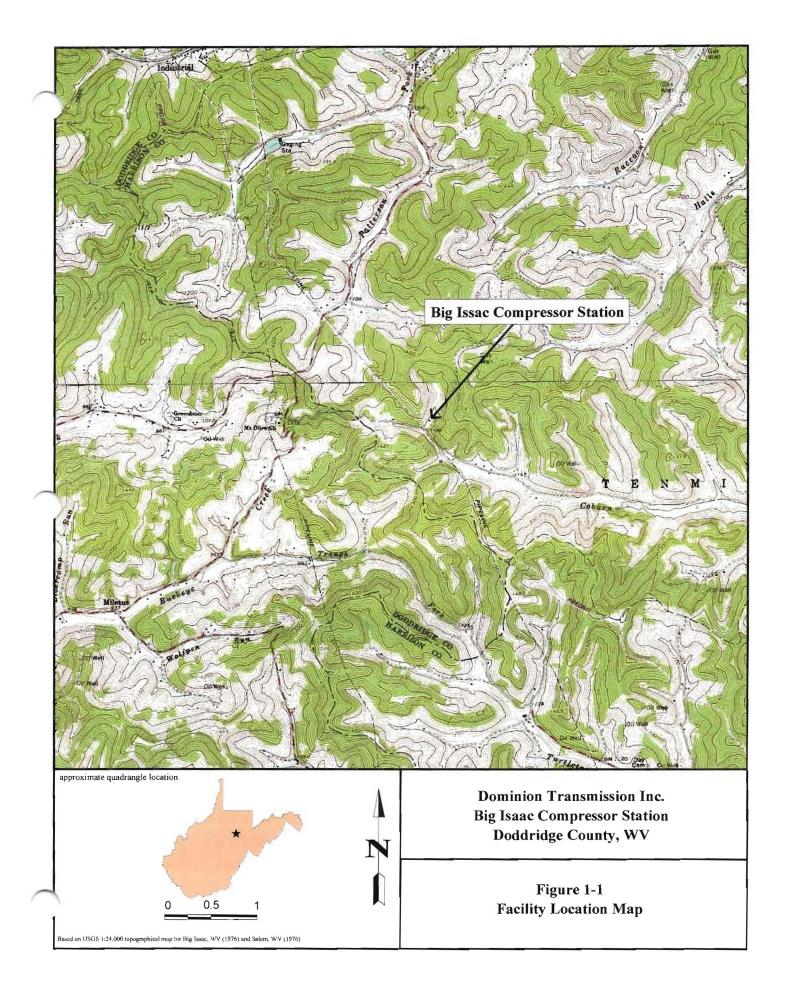


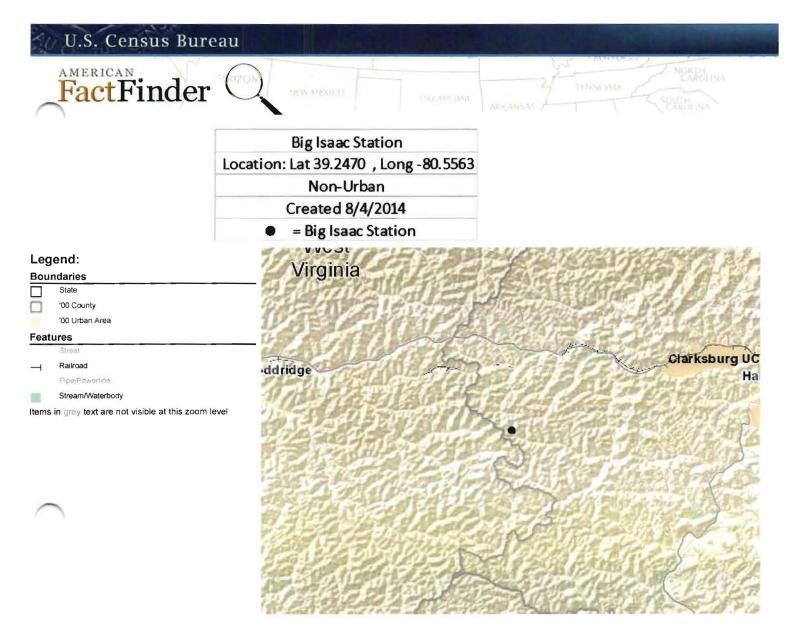
Process Flow Diagram Dominion Transmission, Inc. Big Isaac Compressor Station – Doddridge County, WV

### ATTACHMENT E PLOT PLAN



### ATTACHMENT F AREA MAP





# ATTACHMENT G EQUIPMENT DATA SHEETS

#### General Permit G35-A Registration Section Applicability Form

General Permit G35-A was developed to allow qualified registrants to seek registration for a variety of sources. These sources include internal combustion engines, boilers, reboilers, line heaters, tanks, emergency generators, dehydration units not subject to MACT standards, dehydration units not subject to MACT standards and being controlled by a flare control device, dehydration units not subject to MACT standards and being controlled by recycling the dehydration unit back to flame zone of reboiler, dehydration units not subject to MACT standards being controlled by a thermal oxidizer, and permit exemptions including the less than 1 ton/year benzene exemption, the 40CFR63 Subpart HH - Annual Average Flow of Gas Exemption (10 mmscf/day), and the 40CFR63 Subpart HHH - Annual Average Flow of Gas 4.0.

General Permit G35-A allows the registrant to choose which sections of the permit that they wish to seek registration under. Therefore, please mark which sections that you are applying for registration under. Please keep in mind, that if this registration is approved, the issued registration will state which sections will apply to your affected facility.

Section 5	Reciprocating Internal Combustion Engines (R.I.C.E.)*	$\boxtimes$
Section 6	Boilers, Reboilers, and Line Heaters	$\boxtimes$
Section 7	Tanks	
Section 8	Emergency Generators	$\boxtimes$
Section 9	Dehydration Units Not Subject to MACT Standards	
Section 10	Dehydration Units Not Subject to MACT Standards and being controlled by a flare control device	$\boxtimes$
Section 11	Dehydration Units Not Subject to MACT Standards being controlled by	
Contra you Mitta you	recycling the dehydration unit back to the flame zone of the reboiler	
Section 12	Dehydration Units Not Subject to MACT Standards and being controlled	
	by a thermal oxidizer	
Section 13	Permit Exemption (Less than 1 ton/year of benzene exemption)	$\boxtimes$
Section 14	Permit Exemption (40CFR63 Subpart HH – Annual average flow of	
o	gas exemption (3 mmscf/day))	
Section 15	Permit Exemption (40CFR63 Subpart HHH – Annual average flow of gas exemption (10 mmscf/day))	
Section 16	Standards of Performance for Stationary Spark Ignition Internal	$\boxtimes$
	Combustion Engines (40CFR60 Subpart JJJJ)	_

\* Affected facilities that are subject to Section 5 may also be subject to Section 16. Therefore, if the applicant is seeking registration under both sections, please select both.

## NATURAL GAS COMPRESSOR/GENERATOR ENGINE DATA SHEET

Source Ide	entification Number <sup>1</sup>	<u>CE-1</u>		G	E-1		
Engine Manufacturer and Model		Ajax Model DPC-360 LE		Cummins Power Generation Model WSG-1068			
Manufacturer's Rated bhp/rpm		360/400		97.5	/1800		
Source Status <sup>2</sup>			ES		ĒS		
Date Installe	d/Modified/Removed <sup>3</sup>	12/	1998	20	010		
Engine Manufact	rured/Reconstruction Date <sup>4</sup>	1998	or prior	20	010		
Is this a Certified Engine according (Yes or No) <sup>5</sup>	Stationary Spark Ignition to 40CFR60 Subpart JJJJ?	N		Y	les		
	Engine Type <sup>6</sup>	25	SLB	4S	RB		
	APCD Type <sup>7</sup>	N	one	N	one		
Engine, Fuel and Combustion Data	Fuel Type <sup>8</sup>	<i>I</i>	RG	R	26		
	H <sub>2</sub> S (gr/100 scf)	Negligible		Negligible			
	Operating bhp/rpm	360/400		97.5/1800			
	BSFC (Btu/bhp-hr)	~7,700		N/A			
	Fuel throughput (ft <sup>3</sup> /hr)	~2,222		~861			
	Fuel throughput (MMft <sup>3</sup> /yr)	~19.46		~0.43			
	Operation (hrs/yr)	8,760		500			
Reference <sup>9</sup>	Potential Emissions <sup>10</sup>	lbs/hr	tons/yr	lbs/hr	tons/yr	lbs/hr	tons/yr
MD	NOx	1.59	6.95	2.15	0.54		
MD	СО	0.71	3.13	83.19	20.80		
MD	VOC	0.95	4.17	2.15	0.54		
AP	SO <sub>2</sub>	<0.01	<0.01	<0.01	<0.01		
AP	PM 10	0.11	0.47	0.01	<0.01		
AP	Formaldehyde	0.15	0.67	0.02	<0.01		
AP	Total HAP	0.22	0.97	0.03	<0.01		

 Enter the appropriate Source Identification Number for each natural gas-fueled reciprocating internal combustion compressor/generator engine located at the compressor station. Multiple compressor engines should be designated CE-1, CE-2, CE-3 etc. Generator engines should be designated GE-1, GE-2, GE-3 etc. If more than three (3) engines exist, please use additional sheets.

West Virginia Department of Environmental Protection • Division of Air Quality

2. Enter the Source Status using the following codes:

NS	Construction of New Source (installation)	ES	Existing So

- MS Modification of Existing Source
- ource
- RS Removal of Source
- 3. Enter the date (or anticipated date) of the engine's installation (construction of source), modification or removal.
- 4. Enter the date that the engine was manufactured, modified or reconstructed.
- 5. Is the engine a certified stationary spark ignition internal combustion engine according to 40CFR60 Subpart JJJJ. If so, the engine and control device must be operated and maintained in accordance with the manufacturer's emission-related written instructions. You must keep records of conducted maintenance to demonstrate compliance, but no performance testing is required. If the certified engine is not operated and maintained in accordance with the manufacturer's emission-related written instructions, the engine will be considered a non-certified engine and you must demonstrate compliance according to 40CFR§60.4243a(2)(i) through (iii), as appropriate.

#### Provide a manufacturer's data sheet for all engines being registered.

- 6. Enter the Engine Type designation(s) using the following codes:
  - LB2S Lean Burn Two Stroke RB4S Rich Burn Four Stroke
  - LB4S Lean Burn Four Stroke
- 7. Enter the Air Pollution Control Device (APCD) type designation(s) using the following codes:

	A/F	Air/Fuel Ratio	IR	Ignition Retard
	HEIS	High Energy Ignition System	SIPC	Screw-in Precombustion Chambers
	PSC	Prestratified Charge	LEC	Low Emission Combustion
	NSCR	Rich Burn & Non-Selective Catalytic Reduction	SCR	Lean Burn & Selective Catalytic Reduction
8.	Enter the F	uel Type using the following codes:		
	PQ	Pipeline Quality Natural Gas	RG	Raw Natural Gas
0	Enter the 1	Detential Emissions Data Defension designation opti-	the fe	Hawing and a Attach all referenced data to

9. Enter the Potential Emissions Data Reference designation using the following codes. Attach all referenced data to this Compressor/Generator Data Sheet(s).

MD	Manufacturer's Data	AP	AP-42	
GR	GRI-HAPCalc <sup>TM</sup>	OT	Other	(please list)

10. Enter each engine's Potential to Emit (PTE) for the listed regulated pollutants in pounds per hour and tons per year. PTE shall be calculated at manufacturer's rated brake horsepower and may reflect reduction efficiencies of listed Air Pollution Control Devices. Emergency generator engines may use 500 hours of operation when calculating PTE. PTE data from this data sheet shall be incorporated in the Emissions Summary Sheet.

# NATURAL GAS GLYCOL DEHYDRATION UNIT DATA SHEET

		Manufact	turer and Model	Cameron	n 210/350	
		Max Dry Gas F	low Rate (mmscf/day)	4 mmscfd		
		Design Heat	Input (mmBtu/hr)	0.567 M	MBtu/hr	
		Design Typ	be (DEG or TEG)	TI	EG	
	l Glycol	Sou	rce Status <sup>2</sup>	E	S	
	tion Unit ata	Date Installed/	Modified/Removed <sup>3</sup>	06/01	/2011	
		Regenerator	Still Vent APCD <sup>4</sup>	F		
		Fuel H	IV (Btu/scf)	~1,	248	
		H <sub>2</sub> S Cont	tent (gr/100 scf)	Negligible		
		Opera	tion (hrs/yr)	8,760		
Source ID # <sup>1</sup>	Vent	Reference <sup>5</sup>	Potential Emissions <sup>6</sup>	lbs/hr	tons/yr	
	Reboiler Vent	MD	NO <sub>X</sub>	0.05	0.22	
		MD	СО	0.04	0.18	
<i>RBV-1</i> *		MD	VOC	0.04	0.17	
		AP	SO <sub>2</sub>	<0.01	<0.01	
		AP	PM <sub>10</sub>	<0.01	<0.01	
		GRI-GLYCalc <sup>™</sup>	VOC	2.17	9.55	
	GRI-GLYCalc <sup>™</sup>		Benzene	0.02	0.07	
RSV-1**	Glycol Regenerator	GRI-GLYCalc <sup>™</sup>	Ethylbenzene	0.01	0.06	
ATT 1 - 1	Still Vent	GRI-GLYCalc <sup>™</sup>	Toluene	0.02	0.07	
		GRI-GLYCalc <sup>™</sup>	Xylenes	0.18	0.79	
		GRI-GLYCalc <sup>™</sup>	n-Hexane	0.02	0.07	

- 1. Enter the appropriate Source Identification Numbers for the glycol dehydration unit Reboiler Vent and glycol Regenerator Still Vent. The glycol dehydration unit Reboiler Vent and glycol Regenerator Still Vent should be designated RBV-1 and RSV-1, respectively. If the compressor station incorporates multiple glycol dehydration units, a *Glycol Dehydration Unit Data Sheet* shall be completed for each, using Source Identification #s RBV-2 and RSV-2, RBV-3 and RSV-3, etc.
- 2. Enter the Source Status using the following codes:

NS	Construction of New Source
MS	Modification of Existing Source

ES Existing Source RS Removal of Source

- 3. Enter the date (or anticipated date) of the glycol dehydration unit's installation (construction of source), modification or removal.
- 4. Enter the Air Pollution Control Device (APCD) type designation using the following codes:
  - NA None

CD Condenser

FL Flare

Condenser/Combustion Combination

TO Thermal Oxidizer

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CC

5. Enter the Potential Emissions Data Reference designation using the following codes:

MD	Manufacturer's Data	AP	AP-42	
GR	GRI-GLYCalc <sup>™</sup>	OT	Other	(please list)

6. Enter the Reboiler Vent and glycol Regenerator Still Vent Potential to Emit (PTE) for the listed regulated pollutants in lbs per hour and tons per year. The glycol Regenerator Still Vent potential emissions may be determined using the most recent version of the thermodynamic software model GRI-GLYCalc<sup>™</sup> (Radian International LLC & Gas Research Institute). Attach all referenced Potential Emissions Data (or calculations) and the GRI-GLYCalc Aggregate Calculations Report to this Glycol Dehydration Unit Data Sheet(s). This PTE data shall be incorporated in the Emissions Summary Sheet.

Include a copy of the GRI-GLYCalc<sup>TM</sup> analysis. This includes a printout of the aggregate calculations report, which shall include emissions reports, equipment reports, and stream reports.

\*An explanation of input parameters and examples, when using GRI-GLYCalc<sup>™</sup> is available on our website.

#### West Virginia Department of Environmental Protection

#### Division of Air Quality 40 CFR Part 63; Subpart HH & HHH Registration Form

#### DIVISION OF AIR QUALITY : (304) 926-0475 WEB PAGE: http://www.wvdep.org

Complete this form for any oil and natural gas production or natural gas transmission and storage facility that uses an affected unit under HH/HHH, whether subject or not.

	Section A: Facility Description	
Affected facility actual annual average na		4 mmscf/day
Affected facility actual annual average hy		N/A
	, or stores hydrocarbon liquids prior to custody	transfer. No
The affected facility processes, upgrades,	, or stores natural gas prior to the point at which	ch natural gas Yes
(NG) enters the NG transmission and stor	rage source category or is delivered to the end u	ISEr.
The affected facility is: X prior to a	a NG processing plant 🛛 🗌 a NG proce	essing plant
prior to the point	t of custody transfer and there is no NG process	ing plant
The affected facility transports or stor	res natural gas prior to entering the pipelin	ne to a local No
distribution company or to a final end use	er (if there is no local distribution company).	
The affected facility exclusively processe		No
Initial producing gas-to-oil ratio (GOR):	scf/bbl API gravity:de	egrees
	Section B: Dehydration Unit (if applicable)	I
Description: Cameron	Glycol Dehydration Unit	
Date of Installation: 6/2011	Annual Operating Hours: 8,760	Burner rating (MMbtu/hr): 0.567
Exhaust Stack Height (ft): 25.5	Stack Diameter (ft): 1.10	Stack Temp. (°F): ~1,600
Glycol Type:	TEG EG Other:	:
Glycol Pump Type:	Electric Gas If gas, what is the	volume ratio?ACFM/gpm
Condenser installed?	Yes No Exit Temp.	°F Condenser Pressurepsig
Incinerator/flare installed?	Yes No Destruction Eff.	<u>95 %</u>
Other controls installed?	Yes No Describe:	
Wet Gas <sup>2</sup> : Ga	as Temp.: <u>~110</u> °F Gas Pressure <u>~170</u> ps	sig
(Upstream of Contact Tower) Sa	turated Gas? 🛛 Yes 🗌 No	If no, water content lb/MMSCF
Dry Gas: G	as Flowrate(MMSCFD) Actual I	Design <u>4</u>
(Downstream of Contact Tower) W	Water Content _7_lb/MMSCF	
Lean Glycol: Ci	irculation rate (gpm) Actual <sup>3</sup> Ma	aximum <sup>4</sup> <u>3 gal/lb H2O</u>
Pi	ump make/model:	
Glycol Flash Tank (if applicable): Te	emp.: <u>150</u> °F Pressure <u>60</u> psig Ver	nted? Yes 🗌 No 🖂
	no, describe vapor control: Recycle back to pre	ocess
Stripping Gas (if applicable): So	ource of gas: N/A	Rate scfm

	Please attach the following required dehydration unit information:						
- ···			ormation. See Page 43 of this document for an example of a gas flow schematic. It is not intended that the				
			es. The level of detail that is necessary is to establish where the custody transfer points are located. This can be am indicating custody transfer points and the natural gas flow. However, the DAQ reserves the right to request				
		ation in order to make the ne					
2.	· · · · · · · · · · · · · · · · · · ·						
			should be taken from the inlet gas line, downstream from any inlet separator, and using a manifold to remove				
		(or similar) should be used.	collect the sample from the center of the gas line. GPA standard 2166 reference method or a modified version of				
3.			maximum Lean Glycol circulation rate and maximum throughput.				
4.		s of gas or hydrocarbon flow					
		Sectio	n C: Facility NESHAPS Subpart HH/HHH status				
		Subject to Sul	bpart HH				
A	ffected facility	Subject to Sul	ppart HHH				
	status:	Not Subject	□ < 10/25 TPY				
(ch	oose only one)	because:	Affected facility exclusively handles black oil				
	$\Box$ The facility wide actual annual average NG throughput is < 650 thousand						
	scf/day and facility wide actual annual average hydrocarbon liquid is $< 250$ bpd						
			No affected source is present				

8 of 9		

<b>COMPRESSOR STATION EMISSION SUMMARY SHEET FOR CRITERIA POLLUTANTS</b>										
	Compressor Station						Registration Number (Agency Use) <u>G35-A</u>			
Potential Emissions (lbs/hr)						Potent	ial Emissions	(tons/yr)		
Source ID No.	NOx	со	VOC	SO <sub>2</sub>	PM 10	NOx	со	VOC	SO <sub>2</sub>	PM 10
CE-1	1.59	0.71	0.95	<0.01	0.11	6.95	3.13	4.17	<0.01	0.47
GE-1	2.15	83.19	2.15	<0.01	0.01	0.54	20.80	0.54	<0.01	<0.01
RBV-1	0.05	0.04	0.04	<0.01	<0.01	0.22	0.18	0.17	<0.01	<0.01
RSV-1	-	-	2.17	-	-	-	-	9.55	-	-
FL-2	0.07	0.06	-	-	0.01	0.32	0.27	-	-	0.05
Total	3.86	84.00	5.31	<0.01	0.13	8.03	24.38	14.43	<0.01	0.52

0.01

0.02

0.18

0.02

Total

Г

COMPR	COMPRESSOR STATION EMISSION SUMMARY SHEET FOR HAZARDOUS/TOXIC POLLUTANTS													
	Compressor Station								Registration Number (Agency Use) G35-A					
		Potential Emissions (lbs/hr)							tential Emis	ssions (tons	/yr)			
Source ID No.	Benzene	Ethyl- benzene	Toluene	Xylenes	n- Hexane	Formalde- hyde	Benzene	Ethyl- benzene	Toluene	Xylenes	п- Нехапе	Formalde- hyde		
CE-1	<0.01	<0.01	<0.01	<0.01	<0.01	0.15	0.02	<0.01	0.01	<0.01	<0.01	0.67		
GE-1	<0.01	<0.01	<0.01	<0.01	<0.01	0.02	0.02	<0.01	0.01	<0.01	<0.01	<0.01		
RBV-1	-	-	-	-	-	-	-	-	-	-	-	-		
RSV-1	0.02	0.01	0.02	0.18	0.02	-	0.07	0.06	0.07	0.79	0.07	-		
		L												

0.17

0.11

0.06

0.09

0.79

0.07

0.67

0.02

# ATTACHMENT H AIR POLLUTION CONTROL DEVICE SHEETS

# **Flare System Control Device Sheet**

				General I	nformation				
1) Control Dev	ice ID	#: FL-2			2) Installation	n Date	: March 2015		🛛 New
3) Maximum F	lare Ra	ated Capaci	ty: 32.88	Mscf/day	4) Maximum	Pilot	Rated Capacity:	0.05	MMBtu/hr
				5) Emission U	nit Informatio	o <b>n</b>			
		Lis	t the emission		nissions are con pint ID#: <i>FL-2</i> )		l by this flare:		
Emiss	ion Ur	nit ID#	F	Emission Sourc	e Description		Insta	allation Da	te
RSV – 1					Regeneration	Still	06/01/2011		
									🗌 NEW
									🗌 NEW
				6) Stack I	nformation		blease attach addi	Hea	t Content of
Flare Height	L ip J	Diameter	Stack D	ischarge	Assist Type	Gas Gas			e Gas + Any kiliary Fuel
	1.	10 ft	Horizonta	ıl vith Rain cap	☐ Steam ☐ Air ☐ Pressure ⊠ Non		< <b>60</b> ft/	's >20	00 Bt /sc
25.5 ft									
25.5 ft				7) Flare Fue	el Information				
25.5 ft Type/Grade o Fuel Combusto		Cap	um Fuel acity le units)	7) Flare Fue Heat Co (include	ontent units)	Fu	el Contents	Lim	d Operating itation de units)
Type/Grade o		Cap (includ	acity	Heat Co	ontent units)	Fu % Sul	el Contents fur: <i>negligible</i> h: <i>negligible</i>	Lim (inclu	itation
Type/Grade o Fuel Combusto		Cap (includ	acity le units)	Heat Co (include >200 Bi	ontent units) tu/scf	Fu % Sul	fur: <i>negligible</i>	Lim (inclu	itation de units)
Type/Grade o Fuel Combusto	ed	Cap (includ ~22.8 Maxim Cap	acity le units)	Heat Co (include >200 Bi	ontent units) tu/scf Information ontent	Fu % Sul % Ast	fur: <i>negligible</i>	Lim (inclu N Requeste Lim	itation de units)

# Flare System Control Device Sheet (continued)

9) Control Information									
Pollutant(s) Controlled     % Control Efficiency     Pollutant(s) Controlled     % Control Efficiency									
VOC	95%								
НАР	95%								
If ad	If additional pollutants are being controlled, attach additional information.								
10	) Emission Calculations Attac		] NO						
	Please attach a copy of all emission calculations.								
11	11) Additional Information Attached? 🛛 YES 🗌 NO								
	Please attach a copy of flare manufacturer's data sheet.								

If any of the requested information is not available, please contact the flare manufacturer.

Flares meeting the requirements of G35-A Section 10 and registered under General Permit G35-A are considered federally enforceable.



#### Dominion - Big Isaac OP4 Station

#### Q50 Thermal Oxidizer Emission Estimates

Design Load - GRI-GLYCalc Simulation Data received August 2013

Waste stream	Regenerator Overheads Stream
Flowrate	32.88 mscf/d
Major Components	83.3% H <sub>2</sub> O, 9.75% C <sub>1</sub> , 1.74% C <sub>2</sub>

Flue gas emission estimates based on waste to fuel gas ratio of 1:0.2

Nitrogen Oxides NOx (ppm) NOx (tons/yr)

Sulphur Dioxide SO<sub>2</sub> (ppm) SO<sub>2</sub> (tons/yr)

Carbon Monoxides CO (ppm) CO (tons/yr)

Total Hydrocarbons HCT (ppm) HCT (tons/yr)

Nonmethane Hydrocarbons NMHC (ppm) NMHC (tons/yr)

#### Fuel

Fuel type Typical fuel consumption

#### **Exhaust characteristics**

Exhaust diameter Exhaust height Exhaust temperature Exhaust velocity Questor model number Questor combustion Efficiency less than 60 ppm 0.32 tons/yr

0 ppm 0 tons/yr

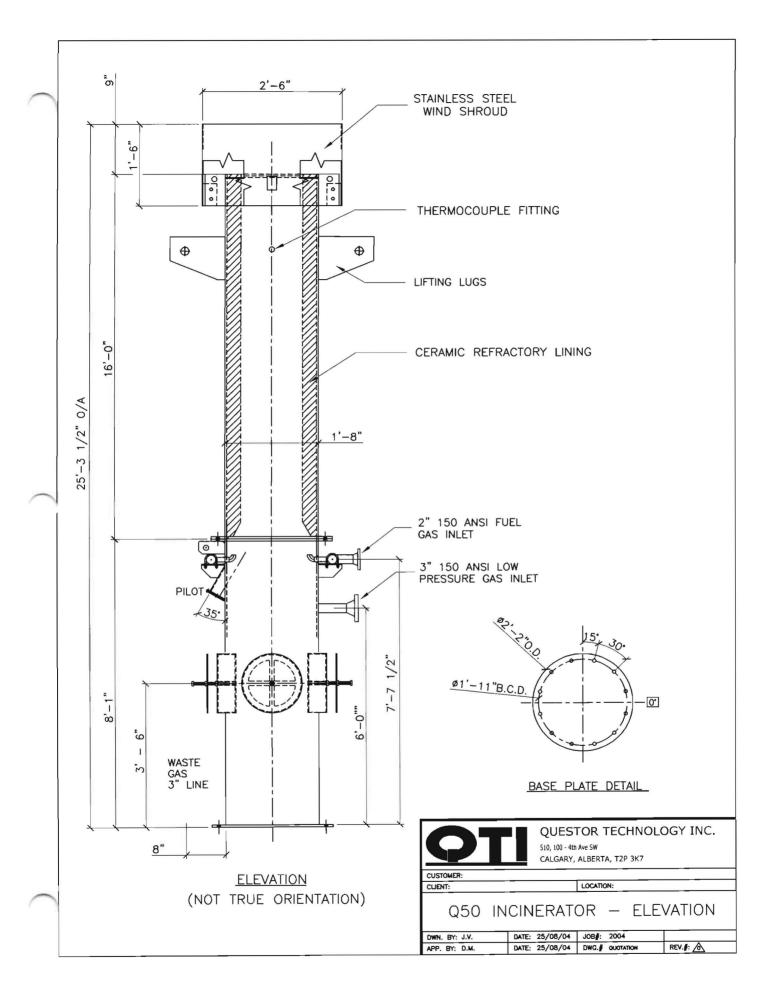
less than 120 ppm 0.27 tons/yr

less than 20 ppm 0.017 tons/yr

less than 20 ppm 0.008 tons/yr

Natural gas (1050 Btu/scf NHV) 5 - 10 mscf/d

13.2 inches 30 Ft from skid base 1112 - 1600°F 16 - 25 ft/sec Q50 Thermal Oxidizer >99.99%





# **QUESTOR Q50 INCINERATOR**

#### **TECHNICAL SPECIFICATIONS**

#### <u>Design Basis</u>

Maximum throughput: Fuel requirement: Design operating temperature:

50,000 scf/d of methane equivalent gas (varies depending upon waste gas composition) 600 to 1200 °C

### **Questor Q50 Incinerator Detail**

Total height: Total weight: Foot print: Number of sections: Stack material: Stack OD: Stack Refractory I.D.: Stack length: Stack wall thickness: Air induction material: Air induction OD: Air induction length: Air induction wall thickness: Wind shroud: Flanges Bolting

25 1/2 feet (7.7 meters) 4,000 lbs (1,814 kg) 2 feet - 3 <sup>3</sup>/<sub>4</sub> inch Dia (0.84 m Dia) 3 - Stack and air induction A36 - Refractory lined 20.0 inches (51 cm) 13.5 inches (34 cm) 16.0 feet (4.9 m) 0.25 inches (6.35 mm) A36 20.0 inches (51 cm) 8 feet - 5 inches (2.5 m) 0.500 inches (12.7 mm) Stainless steel, 2 feet - 6 inches OD **A105 BWRF** A335

#### **Refractory Specification**

Type: Thickness: Manufacturer: Maximum working temperature: 4LI 3 inches Rescocast 2600 °F 1427 °C

#### **Gas Supply Connections**

Waste gas: Pilot gas: Fuel gas: 3 inch 150ANSI RFWN ¼ inch NPT 2 inch 150ANSI RFWN

Page 1 of 1



# **QUESTOR Q50 INCINERATOR**

#### **TECHNICAL SPECIFICATIONS**

#### Combustion Air

Natural draft:

3 openings c/w flame arrestor cells (Optional)

#### **Pilot Gas Burner**

Pilot Ignition Control: Number of Igniters: Capacity at 3 psi: Profire 1100, 1 34 m<sup>3</sup>/d

#### Fuel Gas Burner

Operating Pressure Range: Manifold material: 5 - 7 psig Stainless steel 304

#### Waste Gas Burner

Operating Pressure Range:1 – 40Manifold material:Stainle

1 – 40 psig Stainless steel 304

#### Control Panel - (Solar Power Battery)

NEMA 4, local control panel: lgnition panel:

24 VDC controls NEMA 4 x enclosure

#### Surface Preparation

Sand blast: Top coat: SP6 High temperature aluminum

Page 2 of 2



# **QUESTOR Q50 INCINERATOR**

## **TECHNICAL SPECIFICATIONS**

Stack top temperature:	2 – Alltemp Type K Thermocouple, Inconel 600 & Hastelloy X thermowell 2 – Rosemount 644 Temperature Transmitters
Air intake flame arrestors:	3 – Circular wrapped corrugated aluminum flash Back arrestors 4" thick x 15" diameter 1 – Zirco burner box housing flame arrestor
Inline flame arrestor:	1 - 3" 150ANSI RF flanged, CS body, SS element Flame arrestor
Matching base plate:	1 – $\frac{1}{2}$ " x 2' 3 $\frac{3}{4}$ " plate with matching $\frac{7}{8}$ " bolt holes
Guy Wires	3 - ¾" x 100' guy wires

Questor Technology Inc., Suite 510, 100 - 4th Avenue SW, Calgary, Alberta, Canada, T2P 3N2 Phone: (403) 571 - 1530 Fax: (403) 571 - 1539 http://www.guestortech.com/

# ATTACHMENT I EMISSIONS CALCULATIONS

	Emission Points								
Regulated Pollutant	RSV-1 (Contr	rolled by FL-2)	FL-2 (New)						
	(lb/hr)	(tons/yr)	(lb/hr)	(tons/yr)					
a Cartona Personal	C	riteria Pollutants							
PM <sup>(a)</sup>	-	-	0.01	0.05					
VOC <sup>(b)</sup>	2.17	9.55	-	-					
NOX(c)	-	-	0.07	0.32					
CO <sup>(c)</sup>	-	-	0.06	0.27					
SO <sub>2</sub> <sup>(c)</sup>	-	•	0.00	0.00					
	Greenh	ouse Gas Pollutants <sup>(d)</sup>	and the sure Para line						
CO <sub>2</sub> <sup>(e)</sup>	-	-	77.63	340.95					
CH4 <sup>(f)</sup>	-	-	0.22	0.97					
N <sub>2</sub> O <sup>(g)</sup>	-	-	8.84E-04	3.88E-03					
CO <sub>2</sub> e <sup>(h)</sup>	-	-	83.40	366.29					
	Haza	rdous Air Pollutants							
Total HAP <sup>(b)</sup>	0.24	1.07	-	-					

Table 3-1						
Dominion Transportation - Big Isaac Compressor Station						
<b>Project Related Potential Emissions Summary</b>						

<sup>(a)</sup>Potential emissions of PM include PTE from the combustion of natural gas from the pilot flame and the supplemental natural gas stream, calculated based on the AP-42, Chapter 1 4, Table 1 4-2 emission factor for PM (Total). PM emissions also include PTE from enclosed flare's combustion of emissions from the dehydration still vent and waste fuel gas, calculated based on the AP-42, Chapter 13 5, Table 1 3.5-1 emission factor for soot, assuming a lightly smoking flare (40  $\mu$ g/L). According to the May 2011 Emission Estimation Protocol for Petroleum Refineries, approved by the U.S. EPA on March 28, 2011, 40  $\mu$ g/L is equivalent to 0.027 lb/MMBtu. PM is conservatively assumed to be equivalent to all filterable PM including PM<sub>10</sub> and PM<sub>25</sub>, and condensable fractions

<sup>(b)</sup> Potential emissions of VOC and HAP include PTE from the pilot flame's natural gas combustion, calculated using AP-42 Chapter 1 4, Table 1.4-2 emissions factors for VOC and TOC, and PTE from enclosed flare's combustion of emissions from the dehydration still vent and fuel gas, calculated using GRI-GLYCalc Version 4.0 and an updated gas analysis. The dehydration still vent VOC and HAP emissions represent the sum of controlled regenerator emissions and flash tank off gas emissions generated using GRI-GLYCalc 4.0 with the incorporation of a 20% safety factor. GRI-GLYCalc summaries are included in Appendix B of the Application.

(c)Potential emissions of NO<sub>X</sub>, CO, and SO<sub>2</sub> are based on vendor specifications; maximum flowrate = 32.88 Mscf/day (22.8 scf/min); waste to fuel gas ratio of 1:0.2.

<sup>(d)</sup>Potential emissions of greenhouse gases are calculated from the combustion of natural gas from the pilot flame, the supplemental natural gas stream, and the waste gas in the enclosed flare. Emissions from the supplemental natural gas fuel and the pilot flame natural gas were calculated using a fuel flowrate of 10,000 scf/day and a pilot flame flowrate of 1,200 scf/day to the enclosed flare. Greenhouse gas pollutant emission factors for the combustion of natural gas were obtained from 40 CFR Part 98, Subpart C. The emissions from the combustion of waste gas use the methodologies outlined below:

 ${}^{\rm (e)}\!CO_2$  is calculated assuming emissions from both natural gas and waste gas streams. in metric tons/year,

calculated according to 40 CFR 98 Equation Y-1a, where

$$CO_2 = 0.98 \times 0.001 \times \left(\sum_{p=1}^{n} \left[\frac{44}{12} \times (Flare)_p \times \frac{(MW)_p}{MVC} \times (CC)_p\right]\right)$$

<sup>(1)</sup>CH<sub>4</sub> is in metric tons/year, calculated according to 40 CFR 98 Equation Y-4, where:

$$CH_{4} = \left(CO_{2} \times \frac{EmF_{CH4}}{EmF}\right) + CO_{2} \times \frac{0.02}{0.98} \times \frac{16}{44} \times f_{CH4}$$

<sup>(8)</sup>N<sub>2</sub>O is in metric tons/year, calculated according to 40 CFR 98 Equation Y-5, where

$$N_{2}O = \left(CO_{2} \times \frac{EmF_{N20}}{EmF}\right) \qquad (Eq. Y-5)$$

 $^{(h)}CO_2e$  is carbon dioxide equivalent in metric tons/year, calculated according to 40 CFR 98 Equation A-1, where:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP$$

Table A-1: Global Warming Potentials						
Pollutant	GH'P (100 year)					
CO2	1					
CH4	25					
N <sub>2</sub> O	298					

Flare p = volume flare gas combusted = ~23 acfm.

MW = molecular weight flare gas = 21 kg/kg-mol.

MVC = molar conversion factor of 849 5 scf/kg-mol at 68°F.

CC = carbon concentration of flare gas = 7 87%

0.98 = combustion efficiency of flare (used 0.95 for 95% efficiency)

 $\mathsf{EmF}_{\mathsf{CH4}}$  = Default  $\mathsf{CH}_4$  emission factor for "Fuel Gas" from Table C-2 .

EmF = default CO<sub>2</sub> emission factor for flare gas of 60 kg/CO<sub>2</sub>/MMBtu. CO<sub>2</sub> = emission rate of CO<sub>2</sub> from flared gas in metric tons/year.

 $f_{CH4}$  = default weight fraction of carbon in flare gas of 0.4

0 98 = combustion efficiency of flare (used 0.95 for 95% efficiency)

 $\begin{array}{l} CO_2 = emission \ rate \ of \ CO_2 \ from \ flared \ gas \ in \ metric \ tons/year. \\ EmF_{N2O} = Default \ N_2O \ emission \ factor \ for \ "Fuel \ Gas" \ from \\ Table \ C-2 \ EmF = \ default \ CO_2 \ emission \ factor \ for \ flare \ gas \ of \ 60 \\ kg/CO_2/MMBtu. \end{array}$ 

 $\begin{array}{l} GHG_i=mass\ emissions\ of\ each\ greenhouse\ gas\ listed\ in\ Table \ A-1,\ metric\ tons/year \ GWP_i=global\ warmung\ potential\ for\ each\ greenhouse\ gas\ from \ Table \ A-1. \ n=number\ of\ greenhouse\ gasses\ emitted. \end{array}$ 

# Table 3-2Dominion Transportation - Big Isaac Compressor StationProject Related Changes in Potential Emissions Summary

Regulated Pollutant		Potential E (tons/yr) <sup>(a)</sup>		Project Related Potential Emissions (tons/yr) <sup>(b)</sup>			Change in Potential Emissions (tons/yr) <sup>(c)</sup>			Summary of Changes in Potential Emissions <sup>(d)</sup>	
	RBV-1	RSV-1	FL-1	RBV-1	RSV-1	FL-2	RBV-1	RSV-1	FL-2		
CANCELLAND MARK	Criteria Pollutants										
PM	< 0.01	-	-	< 0.01	-	0.05	< 0.01	-	0.05	0.05	
VOC	0.17	3.97	-	0.17	9.55	-	0.00	5.58	-	5.58	
NO <sub>X</sub>	0.22	-	0.22	0.22	-	0.32	0.00	-	0.1	0.10	
СО	0.18	-	0.70	0.18	-	0.27	0.00	-	0.00	0.00	
SO <sub>2</sub>	< 0.01	-	-	< 0.01	-	-	< 0.01	-	-	0.00	
		A DEL	S S B L	Green	house Gas	Pollutants				AN STREET AND	
CO <sub>2</sub> e	239.17	-	2,485.66	239.17	-	366.29	0.00	-	0.00	0.00	
		300		Haza	rdous Air P	ollutants					
Total HAP	< 0.01	0.71	-	< 0.01	1.07		< 0.01	0.36		0.36	

(a) As reported in Attachment I of the G35-A General Permit application submitted to the West Virginia Department of Environmental Protection (WVDEP) on April 6, 2011.

<sup>(b)</sup> As calculated in Table 3-1 of this G35-A General Permit application.

<sup>(c)</sup> Change in Potential Emissions = ([Project Related Potential Emissions] - [Existing Potential Emissions]).

<sup>(d)</sup> Summary of Changes in Potential Emissions represents the increase in potential emissions from the facility as a result of the proposed project.

Table 3-3Dominion Transportation - Big Isaac Compressor StationFacility-Wide Potential Emission Summary

		Potential Emissions (tons/yr)								
Regulated Pollutant	Existing Ajax Compressor Engine	Existing Auxiliary Generator	Existing Glycol Dehydrator	Existing Reboiler	Proposed Flare	Equipment Fugitives	Total Emissions	Total Emissions Minus Fugitives <sup>(a)</sup>	Title V Thresholds	Title V Facility?
				Criteria Po	llutants					
PM	0.47	2.60E-03	-	3.80E-03	0.05	-	0.53	0.53	100	No
VOC	4.17	0.54	9.55	0.17	~	42.24	56.67	14.43	100	No
NO <sub>X</sub>	6.95	0.54	-	0.22	0.32	-	8.03	8.03	100	No
СО	3.13	20.80	-	0.18	0.27	-	24.37	24.37	100	No
SO <sub>2</sub>	0.01	2.00E-04	-	1.20E-03	-	-	0.01	0.01	100	No
			Gr	eenhouse Ga	s Pollutants	-				
CO <sub>2</sub> e	1,170.00	26.00	-	239.20	366.29	3,293.26	5,094.75	1,801.49	100,000	No
			Н	azardous Air	Pollutants					
Total HAP	0.97	0.01	1.07	0.24	-	1.03	3.32	2.29	25	No

<sup>(a)</sup> Fugitives are not included in Title V applicability.

# ATTACHMENT J CLASS I LEGAL ADVERTISEMENT

-

### **AIR QUALITY PERMIT NOTICE**

### **Notice of Application**

Notice is given that Dominion Transportation, Inc. has applied to the West Virginia Department of Environmental Protection, Division of Air Quality, for a General Permit Registration (G35-A), Modification Permit for the Big Isaac Compressor Station located in Harrison County, West Virginia. The latitude and longitude coordinates are 39.2470° North latitude, -80.5563° East longitude.

The applicant estimates the project's increase in potential to emit (PTE) the following criteria air pollutants will be approximately 0.05 tons per year (tpy) particulate matter (PM), 5.58 tpy volatile organic compounds (VOC), 0.10 tpy nitrogen oxides (NOx), 0.00 tpy carbon monoxide (CO), and 0.00 tpy sulfur dioxide (SO<sub>2</sub>). Additionally, the project's increase in PTE of greenhouse gases (GHG) and hazardous air pollutants (HAP) will be approximately 0.00 tpy and 0.36 tpy, respectively. Startup of operation is planned to begin in March 2015. Written comments will be received by the West Virginia Department of Environmental Protection, Division of Air Quality, 601 57th Street, SE, Charleston, WV 25304, for at least 30 calendar days from the date of publication of this notice.

Any questions regarding this permit application should be directed to the DAQ at (304) 926-0499, extension 1227, during normal business hours. Dated this the (Day) day of (Month), (Year).

By: Dominion Transmission, Inc. Brian Sheppard VP of Pipeline Operations 445 West Main Street Clarksburg, WV 26301

# ATTACHMENT L GENERAL PERMIT REGISTRATION APPLICATION FEE

# APPENDIX B GRI-GLYCALC EMISSION SUMMARY AND WET GAS ANALYSIS

GRI-GLYCalc VERSION 4.0 - AGGREGATE CALCULATIONS REPORT

Case Name: Big Isaac Mountian
'ile Name: M:\Dominion\RFP 02-2014 WV Flare Permitting Projects\GLYCalc\Big Isaac
Mountain\GRI-GLYCalc Big Isaac (11-5-14).ddf
Date: November 25, 2014

#### DESCRIPTION:

Description: GLYCalc PTE Run for Big Isaac Mountain 11-5-14

Annual Hours of Operation: 8760.0 hours/yr

#### EMISSIONS REPORTS:

CONTROLLED REGENERATOR EMISSIONS

Component	lbs/hr	lbs/day	tons/yr
Methane	0.7054	16.929	3.0896
Ethane	0.2134	5.123	0.9349
Propane	0.1581	3.794	0.6925
Isobutane	0.0453	1.087	0.1984
n-Butane	0.0787	1.889	0.3447
Isopentane	0.0370	0.889	0.1623
n-Pentane	0.0319	0.765	0.1395
n-Hexane Cyclohexane Other Hexanes	0.0140 0.0100 0.0185	0.783 0.337 0.241 0.445	0.0614 0.0439 0.0812
Heptanes	0.0515	1.235	0.2254
2,2,4-Trimethylpentane	0.0002	0.006	0.0010
Benzene	0.0142	0.341	0.0622
Toluene	0.0127	0.304	0.0555
Ethylbenzene	0.0110	0.265	0.0484
Xylenes	0.1503	3.607	0.6583
C8+ Heavies	1.1783	28.280	5.1611
Total Emissions	2.7306	65.536	11.9602
Total Hydrocarbon Emissions	2.7306	65.536	11.9602
Total VOC Emissions	1.8118	43.484	7.9358
Total HAP Emissions	0.2025	4.859	0.8868
Total BTEX Emissions	0.1882	4.517	0.8244

#### UNCONTROLLED REGENERATOR EMISSIONS

lbs/hr	lbs/day	tons/yr
ne 14.1077	338.585	61.7917
ine 4.2688	102.452	18.6975
ine 3.1620	75.887	13.8494
ine 0.9060	21.744	3.9683
ine 1.5741	37.779	6.8946
ne 0.7409	17.781	3.2450
ne 0.6371	15.291	2.7905
ne 0.2805	6.732	1.2286
ine 0.2006	4.815	0.8788
nes 0.3709	8.901	1.6245
	ine 14.1077 ine 4.2688 ine 3.1620 ine 0.9060 ine 1.5741 ine 0.7409 ine 0.6371 ine 0.2805 ine 0.2006	$\begin{array}{c} \text{ine} & 14.1077 & 338.585\\ \text{ine} & 4.2688 & 102.452\\ \text{ine} & 3.1620 & 75.887\\ \text{ine} & 0.9060 & 21.744\\ \text{ine} & 1.5741 & 37.779\\ \text{ine} & 0.7409 & 17.781\\ \text{ine} & 0.6371 & 15.291\\ \text{ine} & 0.2805 & 6.732\\ \text{ine} & 0.2006 & 4.815\\ \end{array}$

Page: 1

	Heptanes	1.0290	24.697	4.5072
	2,2,4-Trimethylpentane	0.0047	0.112	0.0204
	Benzene	0.2840	6.816	1.2439
	Toluene	0.2533	6.078	1.1093
	Ethylbenzene	0.2208	5.300	0.9673
	Xylenes	3.0061	72.146	13.1666
	C8+ Heavies	23.5665	565.595	103.2211
	Total Emissions	54.6130	1310.712	239.2049
Tot	al Hydrocarbon Emissions	54.6130	1310.712	239.2049
	Total VOC Emissions	36.2365	869.675	158.7157
	Total HAP Emissions	4.0494	97.184	17.7362
	Total BTEX Emissions	3.7642	90.340	16.4871

Page: 2

FLASH GAS EMISSIONS

Note: Flash Gas Emissions are zero with the Recycle/recompression control option.

FLASH TANK OFF GAS

Component	lbs/hr	lbs/day	tons/yr
Methane Ethane Propane Isobutane n-Butane	0.6269 0.3739 0.2834 0.0804 0.1320	6.802	1.2414
Isopentane n-Pentane n-Hexane Cyclohexane Other Hexanes	0.0607 0.0481 0.0156 0.0036 0.0243	1.154 0.375	0.2106 0.0685
Heptanes 2,2,4-Trimethylpentane Benzene Toluene Ethylbenzene	$\begin{array}{c} 0.0349 \\ 0.0003 \\ 0.0009 \\ 0.0005 \\ 0.0003 \end{array}$		0.1527 0.0011 0.0040 0.0024 0.0013
Xylenes C8+ Heavies	0.0027 0.1318	0.065 3.163	
Total Emissions	1.8204	43.689	7.9733
Total Hydrocarbon Emissions Total VOC Emissions Total HAP Emissions Total BTEX Emissions			3.5894 0.0891

#### EQUIPMENT REPORTS:

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COMBUSTION DEVICE

Page: 3

Ambient Temperature: 68.00 deg. F Excess Oxygen: 5.00 % Combustion Efficiency: 95.00 % Supplemental Fuel Requirement: 2.49e-001 MM BTU/hr

Component	Emitted	Destroyed
Methane Ethane Propane Isobutane n-Butane	5.00% 5.00% 5.00% 5.00% 5.00%	95.00% 95.00% 95.00%
Isopentane n-Pentane n-Hexane Cyclohexane Other Hexanes	5.00% 5.00% 5.00% 5.00% 5.00%	95.00%
Heptanes 2,2,4-Trimethylpentane Benzene Toluene Ethylbenzene	5.00% 5.00% 5.00% 5.00% 5.00%	95.00%
Xylenes C8+ Heavies	5.00% 5.00%	95.00% 95.00%

ABSORBER

÷			
	Calculated Absorber Stages: Specified Dry Gas Dew Point:	1.67 7.00	lbs. H2O/MMSCF
1	Temperature:		deg. F
	Pressure:	170.0	psig
	Dry Gas Flow Rate:	4.0000	MMSCF/day
	Glycol Losses with Dry Gas:	0.0480	lb/hr
	Wet Gas Water Content:	Saturated	
	Calculated Wet Gas Water Content: Specified Lean Glycol Recirc. Ratio:		lbs. H2O/MMSCF gal/lb H2O

Component	Remaining in Dry Gas	Absorbed in Glycol
Water	2.03%	97.97%
Carbon Dioxide	99.79%	0.21%
Nitrogen	99.98%	0.02%
Methane	99.98%	0.02%
Ethane	99.98%	0.06%
Propane	99.88%	0.12%
Isobutane	99.81%	0.19%
n-Butane	99.75%	0.25%
Isopentane	99.70%	0.30%
n-Pentane	99.62%	0.38%
n-Hexane	99.29%	0.71%
Cyclohexane	96.99%	3.01%
Other Hexanes	99.47%	0.53%
Heptanes	98.49%	1.51%
2,2,4-Trimethylpentane	99.27%	0.73%
Benzene	79.45%	20.55%
Toluene	68.84%	31.16%
Ethylbenzene	52.75%	47.25%
Xylenes	41.49%	58.51%
C8+ Heavies	84.77%	15.23%

FLASH TANK			
F	Flash Control Flash Temperature Flash Pressure	: 150	
Componer		eft in Glycol	Removed in Flash Gas
Ca	nrbon Dioxide Nitrogen Methane Ethane Propane Isobutane n-Butane	81.23% 29.09% 30.54% 59.13% 75.14% 81.26% 84.72%	70.91% 69.46% 40.87% 24.86% 18.74% 15.28% 13.81%
2,2,4-Trim	other Hexanes Heptanes Methylpentane Benzene Toluene	93.14% 99.70% 99.80%	1.87% 8.90% 3.79% 6.86% 0.30% 0.20% 0.12%

REGENERATOR

Regenerator Stripping Gas: Dry Product Gas Stripping Gas Flow Rate: 6.9000 scfm

Component	Remaining in Glycol	Distilled Overhead
Water Carbon Dioxide Nitrogen Methane Ethane	7.72% 0.00% 0.00% 0.00% 0.00%	100.00% 100.00%
Propane Isobutane n-Butane Isopentane n-Pentane	0.00% 0.00% 0.58% 0.57%	100.00%
n-Hexane Cyclohexane Other Hexanes Heptanes 2,2,4-Trimethylpentane	0.54% 3.26% 1.10% 0.52% 1.61%	99.46% 96.74% 98.90% 99.48% 98.39%
Benzene Toluene Ethylbenzene Xylenes	5.02% 7.92% 10.42% 12.92%	94.98% 92.08% 89.58% 87.08%

C8+ Heavies 12.06% 87.94% STREAM REPORTS: \_\_\_\_\_ WET GAS STREAM Temperature: 110.00 deg. F Pressure: 184.70 psia Flow Rate: 1.68e+005 scfh nponent Conc. Loading (vol%) (lb/hr) Component Water 7.20e-001 5.74e+001 Carbon Dioxide 1.00e-001 1.95e+001 Nitrogen 1.12e+000 1.39e+002 Methane 7.84e+001 5.57e+003 Ethane 1.13e+001 1.50e+003 Propane 4.76e+000 9.29e+002 Isobutane 8.74e-001 2.25e+002 n-Butane 1.32e+000 3.40e+002 Isopentane 4.61e-001 1.47e+002 n-Pentane 3.43e-001 1.09e+002 n-Hexane 8.14e-002 3.11e+001 Cyclohexane 1.69e-002 6.29e+000 Other Hexanes 1.33e-001 5.08e+001 Heptanes 1.37e-001 6.08e+001 2,2,4-Trimethylpentane 9.93e-004 5.02e-001 Benzene 3.97e-003 1.37e+000 Toluene 1.99e-003 8.10e-001 Ethylbenzene 9.93e-004 4.67e-001 Xylenes 1.09e-002 5.13e+000 C8+ Heavies 2.04e-001 1.53e+002 \_\_\_\_\_ Total Components 100.01 9.35e+003 DRY GAS STREAM \_\_\_\_\_ Temperature: 110.00 deg. F Pressure: 184.70 psia Flow Rate: 1.67e+005 scfh Component Conc. Loading (vol%) (lb/hr) Water 1.47e-002 1.17e+000 Carbon Dioxide 1.01e-001 1.95e+001 Nitrogen 1.13e+000 1.39e+002 Methane 7.90e+001 5.57e+003 Ethane 1.14e+001 1.50e+003 Propane 4.79e+000 9.28e+002 Isobutane 8.79e-001 2.24e+002 n-Butane 1.33e+000 3.39e+002 Isopentane 4.63e-001 1.47e+002 n-Pentane 3.44e-001 1.09e+002

Page: 5

n-Hexane 8.15e-002 3.08e+001 Cyclohexane 1.65e-002 6.10e+000

Page: 6 Other Hexanes 1.33e-001 5.05e+001 Heptanes 1.36e-001 5.99e+001 2,2,4-Trimethylpentane 9.93e-004 4.98e-001 Benzene 3.18e-003 1.09e+000 Toluene 1.38e-003 5.58e-001 Ethylbenzene 5.28e-004 2.46e-001 Xylenes 4.57e-003 2.13e+000 C8+ Heavies 1.74e-001 1.30e+002 \_\_\_\_\_ Total Components 100.00 9.26e+003 LEAN GLYCOL STREAM Temperature: 110.00 deg. F Flow Rate: 2.78e+000 gpm Component Conc. Loading (wt%) (lb/hr) TEG 9.95e+001 1.56e+003 Water 3.00e-001 4.70e+000 Carbon Dioxide 2.61e-013 4.10e-012 Nitrogen 1.43e-013 2.24e-012 Methane 1.93e-018 3.03e-017 Ethane 2.75e-008 4.32e-007 Propane 2.96e-009 4.64e-008 Isobutane 8.21e-010 1.29e-008 n-Butane 1.37e-009 2.14e-008 Isopentane 1.40e-004 2.20e-003 n-Pentane 1.33e-004 2.08e-003 n-Hexane 7.04e-005 1.10e-003 Cyclohexane 3.99e-004 6.25e-003 Other Hexanes 1.74e-004 2.72e-003 Heptanes 2.93e-004 4.60e-003 2,2,4-Trimethylpentane 3.58e-006 5.61e-005 Benzene 9.47e-004 1.49e-002 Toluene 1.38e-003 2.17e-002 Ethylbenzene 1.63e-003 2.56e-002 Xylenes 2.84e-002 4.45e-001 C8+ Heavies 2.03e-001 3.19e+000 \_\_\_\_ Total Components 100.00 1.57e+003

RICH GLYCOL STREAM

Temperature: 110.00 deg. F Pressure: 184.70 psia Flow Rate: 2.96e+000 gpm NOTE: Stream has more than one phase.

 
 Component
 Conc.
 Loading (wt%)

 TEG
 9.40e+001
 1.56e+003

 Water
 3.68e+000
 6.09e+001

 Carbon Dioxide
 2.47e-003
 4.09e-002

 Nitrogen
 1.34e-003
 2.22e-002

 Methane
 5.46e-002
 9.03e-001

 Ethane
 5.53e-002
 9.15e-001

 Propane
 6.89e-002
 1.14e+000
 Isobutane 2.59e-002 4.29e-001 n-Butane 5.22e-002 8.64e-001 Isopentane 2.66e-002 4.39e-001 n-Pentane 2.52e-002 4.17e-001 n-Hexane 1.33e-002 2.21e-001 Cyclohexane 1.18e-002 1.95e-001 Other Hexanes 1.65e-002 2.72e-001 Heptanes 5.56e-002 9.20e-001 2,2,4-Trimethylpentane 2.26e-004 3.74e-003 Benzene 1.80e-002 2.97e-001 Toluene 1.66e-002 2.74e-001 Ethylbenzene 1.49e-002 2.46e-001 Xylenes 2.08e-001 3.45e+000 C8+ Heavies 1.61e+000 2.66e+001 Total Components 100.00 1.65e+003 Page: 7

FLASH TANK OFF GAS STREAM

	Temperature: 150.00 deg. F Pressure: 74.70 psia Flow Rate: 2.50e+001 scfh		
	Component	Conc. (vol%)	Loading (lb/hr)
	Carbon Dioxide Nitrogen Methane	4.74e-001	5.62e-003 7.69e-003 1.58e-002 6.27e-001
	Isobutane n-Butane Isopentane	9.76e+000 2.10e+000 3.45e+000 1.28e+000 1.01e+000	8.04e-002 1.32e-001 6.07e-002
	Cyclohexane Other Hexanes	4.28e-001 5.29e-001	3.65e-003 2.43e-002 3.49e-002
	Toluene Ethylbenzene	3.90e-002 1.18e+000	5.45e-004 2.86e-004 2.72e-003 1.32e-001
	Total Components		
FLAS	SH TANK GLYCOL STREAM		
	Temperature: 150.00 deg. F Flow Rate: 2.96e+000 gpm		
	Component	Conc. (wt%)	Loading (lb/hr)
3		9.41e+001	

Water 3.69e+000 6.09e+001 Carbon Dioxide 2.01e-003 3.33e-002

Nitrogen 3.91e-004 6.46e-003 Methane 1.67e-002 2.76e-001 Ethane 3.27e-002 5.41e-001 Propane 5.18e-002 8.57e-001 Isobutane 2.11e-002 3.49e-001 n-Butane 4.43e-002 7.32e-001 Isopentane 2.29e-002 3.79e-001 n-Pentane 2.23e-002 3.68e-001 n-Hexane 1.24e-002 2.05e-001 Cyclohexane 1.16e-002 1.92e-001 Other Hexanes 1.50e-002 2.48e-001 Heptanes 5.35e-002 8.85e-001 2,2,4-Trimethylpentane 2.11e-004 3.48e-003 Benzene 1.79e-002 2.96e-001 Toluene 1.66e-002 2.74e-001 Ethylbenzene 1.49e-002 2.46e-001 Xylenes 2.09e-001 3.45e+000 C8+ Heavies 1.60e+000 2.64e+001 Total Components 100.00 1.65e+003

FLASH GAS EMISSIONS

Control Method: Recycle/recompression Control Efficiency: 100.00

Note: Flash Gas Emissions are zero with the Recycle/recompression control option.

REGENERATOR OVERHEADS STREAM

Temperature:	212.00	deg.	F
Pressure:	14.70	psīa	
Flow Rate:	1.70e+003	scfh	

Component	Conc. (vol%)	Loading (lb/hr)
Carbon Dioxide Nitrogen Methane	6.96e+001 4.14e-002 2.80e-001 1.96e+001 3.16e+000	8.17e-002 3.52e-001 1.41e+001
Isobutane n-Butane Isopentane	1.60e+000 3.47e-001 6.04e-001 2.29e-001 1.97e-001	9.06e-001 1.57e+000 7.41e-001
Cyclohexane Other Hexanes	9.59e-002 2.29e-001	2.01e-001 3.71e-001 1.03e+000
Toluene Ethylbenzene	6.31e-001	2.53e-001 2.21e-001 3.01e+000

Page: 8

COMBUSTION DEVICE OFF GAS STREAM

Temperature: 1000.00 deg. F		
Pressure: 14.70 psia Flow Rate: 2.56e+001 scfh		
Component		Loading
	(vol%)	(lb/hr)
Methane	6.51e+001	7.05e-001
	1.05e+001	
	5.31e+000	
Isobutane	1.15e+000	4.53e-002
n-Butane	2.01e+000	7.87e-002
Isopentane	7.60e-001	3.70e-002
	6.54e-001	
n-Hexane	2.41e-001	1.40e-002
Cyclohexane		
Other Hexanes	3.19e-001	1.85e-002
Heptanes	7.60e-001	5.15e-002
2,2,4-Trimethylpentane	3.02e-003	2.33e-004
	2.69e-001	
	2.04e-001	
Ethylbenzene	1.54e-001	1.10e-002
Xylenes	2.10e+000	1.50e-001
C8+ Heavies	1.02e+001	1.18e+000
Total Components	100.00	2.73e+000

	Page: 1			
GRI-GLYCalc VERSION 4.0 - SUMMARY OF INPUT VALUES				
Case Name: Big Isaac Mountian 'ile Name: M:\Dominion\RFP 02-2014 WV Flare Permitting Projects\GLYCalc\Big Isaac Mountain\GRI-GLYCalc Big Isaac (11-5-14).ddf Date: November 25, 2014				
DESCRIPTION:				
Description: GLYCalc PTE Run for 11-5-14	Big Isaac Mountain			
Annual Hours of Operation: 87	760.0 hours/yr			
WET GAS:				
Temperature: 110.00 deg. F Pressure: 170.00 psig Wet Gas Water Cont	ent. Saturated			
Component	Conc. (vol %)			
Combon Discuida				
Carbon Dioxide Nitrogen				
Methane	79.0010 2 11.3620			
Ethane	11.3620			
Propane	4.7940			
Isobutane	0.8800			
n-Butane	e 1.3310 e 0.4640			
Isopentane				
	0.3450			
n-Hexane	e 0.0820			
Cyclohexane	e 0.0170			
Other Hexanes	0.1340			
Heptanes 2,2,4-Trimethylpentane	0.1380			
2,2,4-irimetnyipentane Benzene				
Denzene	0.0040			
Toluene	e 0.0020			
Ethylbenzene				
Xylenes				
C8+ Heavies	; 0.2050			
DRY GAS:				
Flow Rate:	4.0 MMSCF/day			
Water Content:	7.0 lbs. H2O/MMSCF			
LEAN GLYCOL:				
	mp/C			
Glycol Type: Water Content:	0.3 wt% H20			
Water Content: Recirculation Ratio:	3.0 gal/lb H2O			
$\bigcirc$				
PUMP :				

Excess Oxygen: 5.0 % Ambient Air Temperature: 68.0 deg. F



#### Certificate of Analysis

Number: 1030-14020696-006A

Houston Laboratories 8820 Interchange Drive Houston, TX 77054 Phone 713-660-0901

Feb. 26, 2014

W. Steven Kiser Dominion Transmission 335 US Highway 33 West Weston , WV 26452

Station Name: Big Isaac StationMethod:GPA 2286Cylinder No:0931Analyzed:02/24/2014 16:32:08 by JD

Sampled By:		
Sample Of:	Gas	Spot
Sample Date:	02/11/2014	4 12:33
Sample Conditions:	176.4 psig	@ 82.7 °F

#### **Analytical Data** Components Mol. % Wt. % GPM at 14.696 psia Nitrogen 1,129 1.504 GPM TOTAL C2+ 5.633 Carbon Dioxide 0.101 0.211 GPM TOTAL C3+ 2.591 Hydrogen Sulfide NIL NIL **GPM TOTAL iC5+** 0.561 Methane 79.001 60.264 3.042 Ethane 11.362 16.245 Propane 4.794 10.052 1.322 Iso-Butane 0.880 2.432 0.288 3.679 1.331 n-Butane 0.420 0.464 Iso-Pentane 0.170 1.592 n-Pentane 0.345 1.184 0.125 0.216 0.895 0.090 Hexanes Heptanes Plus 0.377 1.942 0.176 100.000 100.000 5.633 **Physical Properties** Total C7+ Relative Density Real Gas 3.7442 0.7283 Calculated Molecular Weight 21.03 108.44 Compressibility Factor 0.9964 GPA 2172-09 Calculation: Calculated Gross BTU per ft<sup>3</sup> @ 14.696 psia & 60°F Real Gas Dry BTU 5832 1261 Water Sat, Gas Base BTU 1239 5731 Comments: H2O Mol% : 1.744 ; Wt% : 1.498 H2S 0 ppm

Quality Assurance:

Hydrocarbon Laboratory Manager

The above analyses are performed in accordance with ASTM, UOP, GPA guidelines for quality assurance, unless otherwise stated.



## Certificate of Analysis

Number: 1030-14020696-006A

Houston Laboratories 8820 Interchange Drive Houston, TX 77054 Phone 713-660-0901

Feb. 26, 2014

W. Steven Kiser Dominion Transmission 335 US Highway 33 West Weston , WV 26452

Station Name: Big Isaac StationMethod:GPA 2286Cylinder No:0931Analyzed:02/24/2014 16:32:08 by JD

Sampled By:		
Sample Of:	Gas	Spot
Sample Date:	02/11/201	4 12:33
Sample Conditions	: 176.4 psig	g, @ 82.7 °F

#### **Analytical Data**

	Components	<b>M</b> ol. %	<b>W</b> t. %	GPM at 14.696 psia			
_	Nitrogen	1.129	1.504		GPM TOTAL C2+	5.633	
	Methane	79.001	60.264			0.000	
	Carbon Dioxide	0.101	0.211				
	Hydrogen Sulfide	NIL	NIL				
	Ethane	11.362	16.245	3.042			
	Propane	4.794	10.052	1.322			
	Iso-Butane	0.880	2.432	0.288			
	n-Butane	1.331	3.679	0.420			
	Iso-Pentane	0.464	1.592	0.170			
	n-Pentane	0.345	1.184	0.125			
	i-Hexanes	0.134	0.555	0.056			
	n-Hexane	0.082	0.340	0.034			
1	Benzene	0.004	0.012	0.001			
. )	Cyclohexane	0.017	0.069	0.006			
	i-Heptanes	0.095	0.437	0.042			
	n-Heptane	0.043	0.206	0.020			
	Toluene	0.002	0.009	0.001			
	i-Octanes	0.095	0.492	0.044			
	n-Octane	0.024	0.132	0.013			
	Ethylbenzene	NIL	NIL	NIL			
	Xylenes	0.011	0.058	0.004			
	i-Nonanes	0.039	0.226	0.020			
	n-Nonane	0.015	0.091	0.008			
	i-Decanes	0.019	0.123	0.009			
	n-Decane	0.005	0.034	0.003			
	Undecanes	0.003	0.027	0.002			
	Dodecanes	0.002	0.011	0.001			
	Tridecanes	0.002	0.010	0.001			
	Tetradecanes Plus	0.001	0.005	0.001			
		100.000	100.000	5.633			
	Physical Properties		Tot				
	Calculated Molecular Weig		21.03	30 198.4	13		
	GPA 2172-09 Calculation						
	Calculated Gross BTU pe	er ft <sup>a</sup> @ 14.					
	Real Gas Dry BTU		1260				
	Water Sat. Gas Base BTU		12:				
	Relative Density Real Gas		0.72		00		
	Compressibility Factor		0.996	64			
	Comments: H2S 0 ppm						



Hydrocarbon Laboratory Manager

Quality Assurance:

The above analyses are performed in accordance with ASTM, UOP, GPA guidelines for quality assurance, unless otherwise stated.

# APPENDIX C FLARE DESIGN EVALUATION SHEET

#### Flare Design Evaluation

Туре	Unassisted		
Throat Diameter (inches)	13.5		

	Flowrate (scf/h):	1700	scf/h
GLYCalc	INPUT	Compound Net	Mixture Net
	mole	Heating Value	Heating Value
Compound	percent	(Btu/scf)	(Btu/scf)
Water	69.600	0	0.0
Carbon Dioxide	0.041	0	0.0
Nitrogen	0.280	0	0.0
Methane	19.600	913	178.9
Ethane	3.160	1641	51.9
Propane	1.600	2385	38.2
Isobutane	0.347	3105	10.8
n-Butane	0.604	3113	18.8
Isopentane	0.229	3716	8.5
n-Pentane	0.197	3709	7.3
Cyclopentane	0.000	3516	0.0
n-Hexane	0.073	4412	3.2
Cyclohexane	0.053	4185	2.2
Other Hexanes	0.096	4870	4.7
Heptane	0.229	4925	11.3
2, 2, 4 - Trimethylpentane	0.001	3698	0.0
Benzene	0.081	3601	2.9
Toluene	0.061	4284	2.6
Ethylbenzene	0.046	4977	2.3
Xylene	0.631	4980	31.4
Octane (C8+)	3.080	5804	178.8
Hydrogen Sulfide	0.000	596	0.0
TOTALS:	100		553.8

#### Assist gas requirements for nonassisted flare per 40 CFR 60.18(c)(3):

Minimum allowable net heating value	200	Btw/scf
Additional assist gas required	0.0	scfh
Assist (fuel) gas supplied	0	scfh
Composite net heating value	553.8	Btw/scf

#### Maximum allowable flare exit velocity (V<sub>max</sub>) for nonassisted flare per 40 CFR 60.18(f)(5):

Lower (Net) Heating Value	Btu/scf	MJ/scm
(1000 Btu/scf = 37.3 MJ/scm)	554	20.7
$V_{max} = 10^{[(LHV+28.2)/31.7]}$ for $V_{max}$ in m/sec and LHV in MJ/scm	m/sec	ft/sec
(1 m = 3.28 ft)	36.3	119.1
Vmax limit based on 40 CFR 60.18(b)(4)(iii)	36.3	119.1

#### Actual flare exit velocity:

Total volumetric flow (vent gas + assist gas in scfh/3600 sec/hr) =	0.47	scf/sec
Total volumetric flow at 180F & atmospheric pressure =	0.61	cf/sec
Flare exit cross-sectional area based on throat diameter =	0.99	ft2
Velocity = volumetric flow / cross-sectional area =	0.6	ft/sec